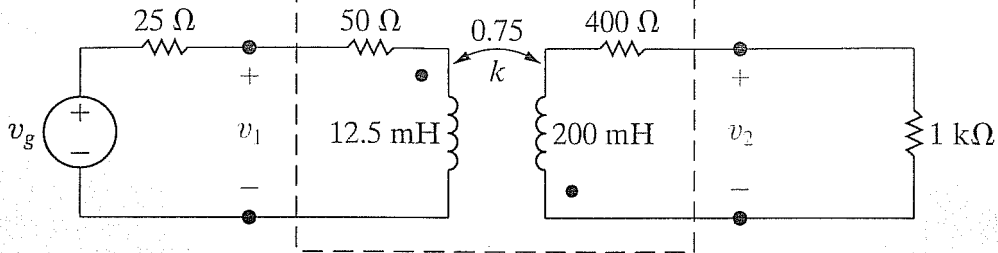


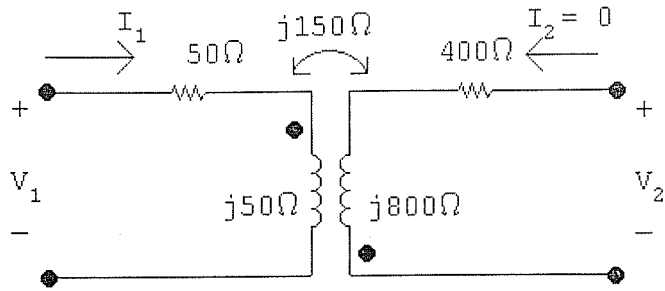
**18.29** The linear transformer in the circuit shown in Fig. P18.29 has a coefficient of coupling of 0.75. The transformer is driven by a sinusoidal voltage source whose internal voltage is  $v_g = 260 \cos 4000t$  V. The internal impedance of the source is  $25 + j0 \Omega$ .

- a) Find the frequency-domain  $a$  parameters of the linear transformer.
- b) Use the  $a$  parameters to derive the Thévenin equivalent circuit with respect to the terminals of the load.
- c) Derive the steady-state time-domain expression for  $v_2$ .

Figure P18.29



P 18.29 [a] For  $I_2 = 0$ :

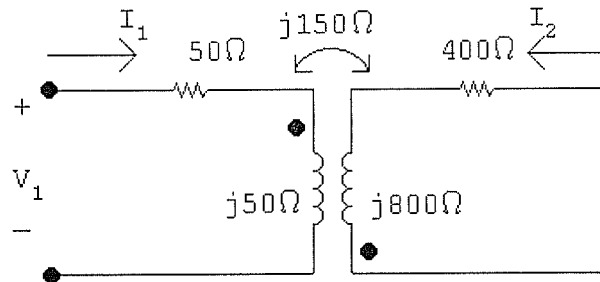


$$V_2 = -j150I_1 = -j150 \frac{V_1}{50 + j50} = \frac{-j3V_1}{1 + j1}$$

$$a_{11} = \left. \frac{V_1}{V_2} \right|_{I_2=0} = \frac{1 + j1}{-j3} = \frac{-1 + j1}{3}$$

$$a_{21} = \left. \frac{I_1}{V_2} \right|_{I_2=0} = \frac{1}{-j150} = \frac{j}{150} \text{ S}$$

For  $V_2 = 0$ :



$$V_1 = (50 + j50)I_1 - j150I_2$$

$$0 = -j150I_1 + (400 + j800)I_2$$

$$\Delta = \begin{vmatrix} 50 + j50 & -j150 \\ -j150 & 400 + j800 \end{vmatrix} = 2500(1 + j24)$$

$$N_2 = \begin{vmatrix} 50 + j50 & V_1 \\ -j150 & 0 \end{vmatrix} = j150V_1$$

$$I_2 = \frac{N_2}{\Delta} = \frac{j150V_1}{2500(1 + j24)}$$

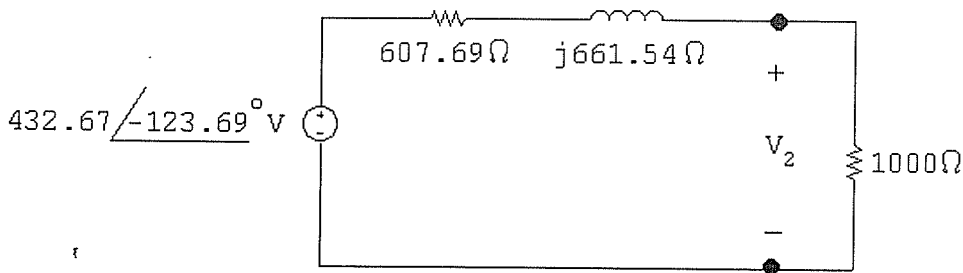
$$a_{12} = \left. \frac{-V_1}{I_2} \right|_{V_2=0} = \frac{-50}{3}(24 - j1) \Omega$$

$$j150I_1 = (400 + j800)I_2$$

$$a_{22} = -\frac{I_1}{I_2} \Big|_{V_2=0} = -\frac{8}{3}(2 - j1)$$

$$\begin{aligned} \text{[b]} \quad V_{\text{Th}} &= \frac{V_g}{a_{11} + a_{21}Z_g} = \frac{260\angle 0^\circ}{(-1 + j1)/3 + j25/150} = \frac{(260\angle 0^\circ)6}{-2 + j2 + j1} = \frac{1560\angle 0^\circ}{-2 + j3} \\ &= 120(-2 - j3) = 432.67\angle -123.69^\circ \text{ V} \end{aligned}$$

$$\begin{aligned} Z_{\text{Th}} &= \frac{a_{12} + a_{22}Z_g}{a_{11} + a_{21}Z_g} = \frac{[-(50/3)(24 - j1)] + [(-8/3)(2 - j1)(25)]}{[(-1 + j1)/3] + [(j/150)(25)]} \\ &= \frac{-100(24 - j1) - 16(2 - j1)(25)}{-2 + j2 + j1} = \frac{-3200 + j500}{-2 + j3} \\ &= 607.69 + j661.54 \Omega \end{aligned}$$



$$\text{[c]} \quad V_2 = \frac{1000}{1607.69 + j661.54} (432.67\angle -123.69^\circ) = 248.88\angle -146.06^\circ$$

$$v_2(t) = 248.88 \cos(4000t - 146.06^\circ) \text{ V}$$

**18.31** The  $b$  parameters for the two-port circuit in Fig. P18.31 are

$$b_{11} = 1 + j\frac{1}{3}; \quad b_{12} = -1 + j4 \Omega;$$

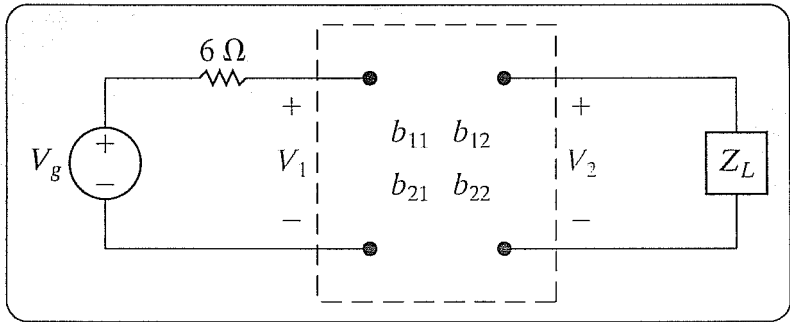
$$b_{21} = \frac{1}{3} \text{ S}; \quad b_{22} = 1 + j1.$$

The load impedance  $Z_L$  is adjusted for maximum average power transfer to  $Z_L$ . The ideal voltage source is generating a sinusoidal voltage of

$$v_g = 90 \cos 8000t \text{ V}.$$

- Find the rms value of  $V_2$ .
- Find the average power delivered to  $Z_L$ .
- What percentage of the average power developed by the ideal voltage source is delivered by  $Z_L$ ?

Figure P18.31



$$\text{P 18.31 [a]} \quad Z_{\text{Th}} = \frac{b_{11}Z_g + b_{12}}{b_{21}Z_g + b_{22}}$$

$$b_{11}Z_g = 6 + j2; \quad b_{21}Z_g = 2$$

$$\therefore Z_{\text{Th}} = \frac{6 + j2 - 1 + j4}{2 + 1 + j1} = \frac{5 + j6}{3 + j1} = 2.1 + j1.3 \Omega$$

$$Z_L = Z_{\text{Th}}^* = 2.1 - j1.3 \Omega$$

$$\frac{V_2}{V_g} = \frac{\Delta b Z_L}{b_{12} + b_{11}Z_g + b_{22}Z_L + b_{21}Z_g Z_L}$$

$$\Delta b = \frac{3 + j1}{3}(1 + j1) - (-1 + j4)(1/3) = 1$$

$$b_{11}Z_g = 6 + j2$$

$$b_{22}Z_L = (1 + j1)(2.1 - j1.3) = 3.4 + j0.8$$

$$b_{21}Z_g Z_L = 4.2 - j2.6$$

$$\frac{V_2}{V_g} = \frac{2.1 - j1.3}{-1 + j4 + 6 + j2 + 3.4 + j0.8 + 4.2 - j2.6} = \frac{2.1 - j1.3}{12.6 + j4.2}$$

$$\therefore V_2 = \frac{2.1 - j1.3}{12.6 + j4.2} (90/0^\circ) = 10.71 - j12.86 = 16.74 / -50.19^\circ \text{ V}$$

$$V_2(\text{rms}) = \frac{16.74}{\sqrt{2}} = 11.84 \text{ V}$$

$$\text{[b]} \quad I_2 = \frac{-(10.71 - j12.86)}{2.1 - j1.3} = 6.78 / 161.57^\circ \text{ A}$$

$$I_2(\text{rms}) = \frac{6.78}{\sqrt{2}} = 4.79 \text{ A}$$

$$P = (4.79)^2(2.1) = 48.21 \text{ W}$$

$$\text{[c]} \quad \frac{I_2}{I_1} = \frac{-\Delta b}{b_{11} + b_{21}Z_L}$$

$$\frac{-1}{(3 + j1)/3 + (2.1 - j1.3)/3} = \frac{-3}{5.1 - j0.3}$$

$$\therefore \frac{I_1}{I_2} = \frac{5.1 - j0.3}{-3} = -1.7 + j0.1$$

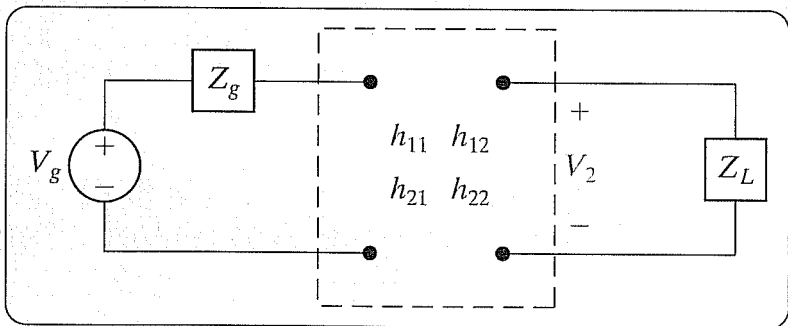
$$I_1 = (-1.7 + j0.1)(6.78 \underline{/161.57^\circ}) = 11.54 \underline{/ - 21.80^\circ} \text{ A}$$

$$P_g \text{ (dev)} = \frac{1}{2} (11.54)(90) \cos(21.80^\circ) = 482.15 \text{ W}$$

$$\% = \frac{48.21}{482.15} (100) \cong 10\%$$



**Figure P18.32**



**18.33** For the terminated two-port amplifier circuit in Fig. P18.32, find

- the value of  $Z_L$  for maximum average power transfer to  $Z_L$
- the maximum average power delivered to  $Z_L$
- the average power developed by the ideal voltage source when maximum power is delivered to  $Z_L$ .

$$\text{P 18.33 [a]} \quad Z_{\text{Th}} = \frac{Z_g + h_{11}}{h_{22}Z_g + \Delta h}$$

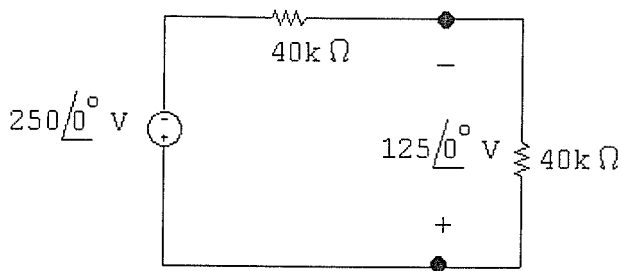
$$\Delta h = (500)(50 \times 10^{-6}) - 50 \times 10^{-3} = -25 \times 10^{-3}$$

$$h_{22}Z_g = 50 \times 10^{-6}(1500) = 75 \times 10^{-3}$$

$$Z_{\text{Th}} = \frac{2000}{75 \times 10^{-3} - 25 \times 10^{-3}} = 40,000 + j0 \Omega$$

$$Z_{\text{L}} = Z_{\text{Th}}^* = 40 + j0 \text{ k}\Omega$$

$$\text{[b]} V_{\text{Th}} = \frac{-h_{21}V_g}{50 \times 10^{-3}} = \frac{-50(250) \times 10^{-3}}{50 \times 10^{-3}} = -250 \text{ V}$$



$$P = \frac{1}{2} \frac{(125)^2}{40,000} = 196.3125 \text{ mW}$$

$$\text{[c]} I_2 = \frac{125}{40,000} = 3.125 \text{ mA}$$

$$\frac{I_2}{I_1} = \frac{h_{21}}{1 + h_{22}Z_L} = \frac{50}{1 + (50 \times 10^{-6})(40,000)} = \frac{50}{3}$$

$$\frac{I_1}{I_2} = \frac{3}{50} = 0.06$$

$$I_1 = 0.06I_2 = 187.5 \mu\text{A}$$

$$P_g (\text{dev}) = \frac{1}{2} (250)(187.5) \times 10^{-6} = 23.4375 \text{ mW}$$

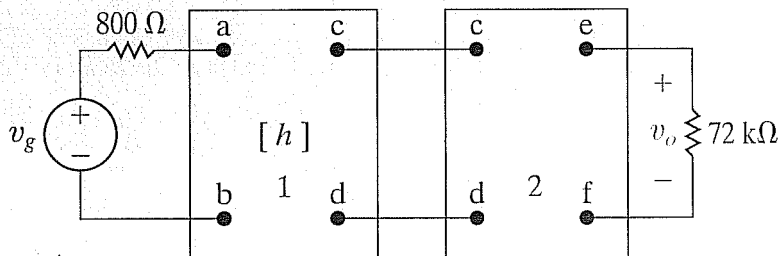
**18.39** The  $h$  parameters of the first two-port circuit in Fig. P18.39(a) are

$$h_{11} = 1000 \Omega; \quad h_{12} = 5 \times 10^{-4};$$

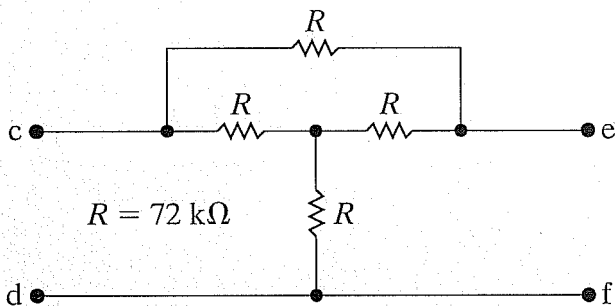
$$h_{21} = 40; \quad h_{22} = 25 \mu\text{S}.$$

The circuit in the second two-port circuit is shown in Fig. P18.39(b), where  $R = 72 \text{ k}\Omega$ . Find  $v_o$  if  $v_g = 9 \text{ mV dc}$ .

**Figure P18.39**



(a)



(b)

P 18.39 The  $a$  parameters of the first two-port are

$$a'_{11} = \frac{-\Delta h}{h_{21}} = \frac{-5 \times 10^{-3}}{40} = -125 \times 10^{-6}$$

$$a'_{12} = \frac{-h_{11}}{h_{21}} = \frac{-1000}{40} = -25 \Omega$$

$$a'_{21} = \frac{-h_{22}}{h_{21}} = \frac{-25}{40} \times 10^{-6} = -625 \times 10^{-9} \text{ S}$$

$$a'_{22} = \frac{-1}{h_{21}} = \frac{-1}{40} = -25 \times 10^{-3}$$

The  $a$  parameters of the second two-port are

$$a''_{11} = \frac{5}{4}; \quad a''_{12} = \frac{3R}{4}; \quad a''_{21} = \frac{3}{4R}; \quad a''_{22} = \frac{5}{4}$$

$$\text{or } a''_{11} = 1.25; \quad a''_{12} = 54 \text{ k}\Omega; \quad a''_{21} = \frac{1}{96} \text{ mS}; \quad a''_{22} = 1.25$$

The  $a$  parameters of the cascade connection are

$$a_{11} = -125 \times 10^{-6}(1.25) + (-25)(10^{-3}/96) = \frac{-10^{-2}}{24}$$

$$a_{12} = -125 \times 10^{-6}(54 \times 10^3) + (-25)(1.25) = -38 \Omega$$

$$a_{21} = -625 \times 10^{-9}(1.25) + (-25 \times 10^{-3})(10^{-3}/96) = \frac{-10^{-4}}{96} \text{ S}$$

$$a_{22} = -625 \times 10^{-9}(54 \times 10^3) + (-25 \times 10^{-3})(1.25) = -65 \times 10^{-3}$$

$$\frac{V_o}{V_g} = \frac{Z_L}{(a_{11} + a_{21}Z_g)Z_L + a_{12} + a_{22}Z_g}$$

$$a_{21}Z_g = \frac{-10^{-4}}{96}(800) = \frac{-10^{-2}}{12}$$

$$a_{11} + a_{21}Z_g = \frac{-10^{-2}}{24} + \frac{-10^{-2}}{12} = \frac{-10^{-2}}{8}$$

$$(a_{11} + a_{21}Z_g)Z_L = \frac{-10^{-2}}{8}(72,000) = -90$$

$$a_{22}Z_g = -65 \times 10^{-3}(800) = -52$$

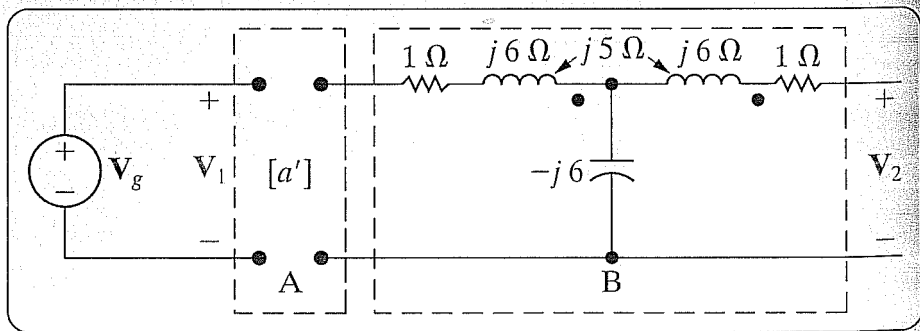
$$\frac{V_o}{V_g} = \frac{72,000}{-90 - 38 - 52} = -400$$

$$v_o = V_o = -400V_g = -3.6 \text{ V}$$

**18.40** The networks A and B in the circuit in Fig. P18.40 are reciprocal and symmetric. For network A, it is known that  $a'_{11} = 2$  and  $a'_{12} = 1 \Omega$ .

- Find the  $a$  parameters of network B.
- Find  $V_2$  when  $V_g = 75 \angle 0^\circ \text{ V}$ ,  
 $Z_g = 1 \angle 0^\circ \Omega$ , and  $Z_L = 14 \angle 0^\circ \Omega$ .

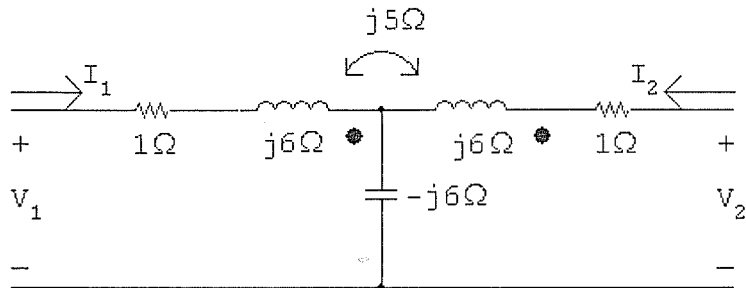
**Figure P18.40**



P 18.40 [a] From reciprocity and symmetry

$$a'_{11} = a'_{22}, \quad \Delta a' = 1; \quad \therefore 4 - a'_{21} = 1, \quad a'_{21} = 3 \text{ S}$$

For network B



$$a''_{11} = \left. \frac{V_1}{V_2} \right|_{I_2=0}$$

$$V_1 = (1 + j6 - j6)\mathbf{I}_1 = \mathbf{I}_1$$

$$V_2 = (-j5 - j6)\mathbf{I}_1 = -j11\mathbf{I}_1$$



$$a''_{11} = \frac{1}{-j11} = \frac{j}{11}$$

$$a''_{21} = \frac{\mathbf{I}_1}{\mathbf{V}_2} \Big|_{I_2=0} = \frac{1}{-j11} = \frac{j}{11} \text{ S}$$

$$a''_{22} = a''_{11} = \frac{j}{11}$$

$$\Delta a'' = 1 = (j/11)(j/11) - (j/11)a''_{12}$$

$$\therefore a''_{12} = \frac{122}{11}j$$

$$\mathbf{[b]} \quad a_{11} = a'_{11}a''_{11} + a'_{12}a''_{21} = 2(j/11) + 1(j/11) = j3/11$$

$$a_{12} = a'_{11}a''_{12} + a'_{12}a''_{22} = 2(j122/11) + 1(j/11) = j245/11$$

$$a_{21} = a'_{21}a''_{11} + a'_{22}a''_{21} = 3(j/11) + 2(j/11) = j5/11$$

$$a_{22} = a'_{21}a''_{12} + a'_{22}a''_{22} = 3(j122/11) + 2(j/11) = j368/11$$

$$I_2 = \frac{-V_g}{a_{11}Z_L + a_{12} + a_{21}Z_gZ_L + a_{22}Z_g} = j1.14$$

$$V_2 = -14I_2 = -j15.9 \text{ V}$$