

American University of Beirut
Faculty of Engineering and Architecture

Spring 2014

Quiz 2

Profs:

Joseph Costantine

Shahwan Khoury

Student Name:

ID number:

Test ID 1001-1002

Section:

EECE 380- Engineering Electromagnetics

CLOSED BOOK Exam:

- Programmable Calculators are not allowed
- Provide your answers to the multiple choice questions on the computer card only
- Provide your answers to the comprehensive problems on the exam sheet

Section I: Multiple Choice Questions (40 pts- 8 pts each)

MCQ 1:

At Cartesian point (-3, 4,-1) which of these is incorrect:

- a. $\rho = -5$
- b. $r = \sqrt{26}$
- c. $\theta = \tan^{-1}\left(\frac{5}{-1}\right)$
- d. $\phi = \tan^{-1}\left(\frac{4}{-3}\right)$

Complete Solution

a.

MCQ 2:

If $\vec{E} = 4\hat{a}_\rho - 3\hat{a}_\phi + 5\hat{a}_z$ at $(1, \pi/2, 0)$, the component of \vec{E} parallel to surface $\rho=1$ is:

- a. $4\hat{a}_\rho$
- b. $5\hat{a}_z$
- c. $-3\hat{a}_\phi$
- d. $-3\hat{a}_\phi + 5\hat{a}_z$
- e. $5\hat{a}_\phi + 3\hat{a}_z$

Complete Solution

d.

MCQ 3:

Point charges $Q_1 = 1$ nC and $Q_2 = 2$ nC are at a distance apart. Which of the following statements is incorrect?

- a. The force on Q_1 is repulsive
- b. The force on Q_2 is the same in magnitude as that on Q_1
- c. As the distance between them decreases, the force on Q_1 increases linearly
- d. The force on Q_2 is along the line joining them
- e. None of the above

Complete Solution

C

MCQ 4:

Point charges Q_1 and Q_2 are, respectively, located at $(4, 0, -3)$ and $(2, 0, 1)$. If $Q_2 = 4 \text{ nC}$, find Q_1 such that the electric field at $(5, 0, 6)$ has no Z component.

- a. $Q_1 = -5.4 \text{ nC}$
- b. $Q_1 = -3.33 \text{ nC}$
- c. $Q_1 = -8.323 \text{ nC}$
- d. $Q_1 = -2.53 \text{ nC}$
- e. $Q_1 = -10.34 \text{ nC}$

Complete Solution

$$\begin{aligned} E(5,0,6) &= \frac{Q_1}{4\pi\epsilon_0} \frac{[(5,0,6)-(4,0,-3)]}{|(5,0,6)-(4,0,-3)|^3} + \frac{Q_2}{4\pi\epsilon_0} \frac{[(5,0,6)-(2,0,1)]}{|(5,0,6)-(2,0,1)|^3} \\ &= \frac{Q_1}{4\pi\epsilon_0} \frac{(1,0,9)}{(\sqrt{82})^3} + \frac{Q_2}{4\pi\epsilon_0} \frac{(3,0,5)}{(34)^{3/2}} \end{aligned}$$

If $E_z = 0$, then

$$\begin{aligned} \frac{9Q_1}{4\pi\epsilon_0} \frac{1}{(82)^{3/2}} + \frac{5Q_2}{4\pi\epsilon_0} \frac{1}{(34)^{3/2}} &= 0 \\ Q_1 &= -\frac{5}{9} Q_2 \left(\frac{82}{34}\right)^{3/2} = -\frac{5}{9} 4 \left(\frac{82}{34}\right)^{3/2} \text{ nC} \\ &= \underline{\underline{-8.3232 \text{ nC}}} \end{aligned}$$

MCQ 5:

A can of tomatoes is in the form of a wedge that is defined by $0 < \rho < 2$, $0 < \Phi < \pi/4$, $0 < z < 1$. Given that the wedge has a volume charge distribution $\rho_v = 4\rho^2 z \cos\phi \text{ nC/m}^3$, find the total charge contained in the wedge.

- a. $Q = 6.754 \text{ nC}$
- b. $Q = 5.657 \text{ nC}$
- c. $Q = 7.856 \text{ nC}$
- d. $Q = 9.324 \text{ nC}$
- e. None of the above

Complete Solution

$$\begin{aligned} Q &= \int_V \rho_v dv = \iiint 4\rho^2 z \cos\phi \rho d\rho d\phi dz \quad \text{nC} \\ &= 4 \int_0^2 \rho^3 d\rho \int_0^1 z dz \int_0^{\pi/4} \cos\phi d\phi = \rho^4 \Big|_0^2 \frac{z^2}{2} \Big|_0^1 (\sin\phi) \Big|_0^{\pi/4} \\ &= (16)(0.5)(\sin\pi/4) = \underline{\underline{5.657 \text{ nC}}} \end{aligned}$$

MCO 7:

Find the electric field at point P(0, 0, 8 m) resulting from a surface charge density $\rho_s = 5 \text{ nC/m}^2$ existing on the $z=0$ plane from $\rho=2$ m to $\rho=6$ m.

- a. $\vec{E} = 24\hat{a}_z \text{ V/m}$
- b. $\vec{E} = 12\hat{a}_z \text{ V/m}$
- c. $\vec{E} = 16\hat{a}_z \text{ V/m}$
- d. $\vec{E} = 8\hat{a}_z \text{ V/m}$
- e. $\vec{E} = 48\hat{a}_z \text{ V/m}$

Complete Solution

Find an expression for potential and then evaluate the gradient at the point.

$$V = \int \frac{dQ}{4\pi\epsilon_0 R}, \quad R = \sqrt{\rho^2 + h^2}, \quad dQ = \rho_s \rho d\rho d\phi, \quad \text{so } V = \int \frac{\rho_s \rho d\rho d\phi}{4\pi\epsilon_0 \sqrt{\rho^2 + h^2}}$$

$$V = \frac{\rho_s}{2\epsilon_0} \int_a^b \frac{\rho d\rho}{\sqrt{\rho^2 + h^2}} = \frac{\rho_s}{2\epsilon_0} \sqrt{\rho^2 + h^2} \Big|_a^b = \frac{\rho_s}{2\epsilon_0} \left[\sqrt{b^2 + h^2} - \sqrt{a^2 + h^2} \right].$$

Now we let $h = z$ and $\mathbf{E} = -\nabla V$;

$$\begin{aligned} \mathbf{E} &= -\frac{\rho_s}{2\epsilon_0} \left[\frac{\partial}{\partial z} (b^2 + z^2)^{1/2} - \frac{\partial}{\partial z} (a^2 + z^2)^{1/2} \right] \mathbf{a}_z \\ &= -\frac{\rho_s}{2\epsilon_0} \left[\frac{1}{2} (b^2 + z^2)^{-1/2} 2z - \frac{1}{2} (a^2 + z^2)^{-1/2} 2z \right] \mathbf{a}_z = -\frac{\rho_s}{2\epsilon_0} \left[\frac{z}{\sqrt{b^2 + z^2}} - \frac{z}{\sqrt{a^2 + z^2}} \right] \mathbf{a}_z \end{aligned}$$

Plugging in the values we find $\mathbf{E} = 48 \text{ V/m } \mathbf{a}_z$.

MCO 8:

Two point charges $Q=2 \text{ nC}$ and $Q=-4 \text{ nC}$ are located at $(1, 0, 3)$ and $(-2, 1, 5)$, respectively. Determine the potential at $P(1, -2, 3)$

- a. $V=1.235 \text{ V}$
- b. $V=1.325 \text{ V}$
- c. $V=3.125 \text{ V}$
- d. $V=5.312 \text{ V}$
- e. $V=2.315 \text{ V}$

Complete Solution

$$V_p = \frac{Q_1}{4\pi\epsilon_0 r_1} + \frac{Q_2}{4\pi\epsilon_0 r_2} = \frac{10^{-9}}{4\pi \times \frac{10^{-9}}{36\pi}} \left[\frac{2}{|(1, -2, 3) - (1, 0, 3)|} - \frac{4}{|(1, -2, 3) - (-2, 1, 5)|} \right]$$

$$= 9 \left[\frac{2}{2} - \frac{4}{\sqrt{9+9+4}} \right] = \underline{\underline{1.325 \text{ V}}}$$

Section II: Comprehensive Problems**Problem 1 (20 pts):**

In a region in free space, the electric flux density is found to be:

$$D = \begin{cases} \rho_0(Z+d)\hat{a}_z \text{ C/m}^2 & (-2d \leq z < 0) \\ -\rho_0(Z-2d)\hat{a}_z \text{ C/m}^2 & (0 \leq z \leq 2d) \end{cases}$$

Everywhere else $D=0$.

- a) Find the volume charge density ρ_v as a function of position everywhere (5 pts)

Using $\nabla \cdot \mathbf{D} = \rho_v$, find the volume charge density as a function of position everywhere:
Use

$$\rho_v = \nabla \cdot \mathbf{D} = \frac{dD_z}{dz} = \begin{cases} \rho_0 & (-2d \leq z \leq 0) \\ -\rho_0 & (0 \leq z \leq 2d) \end{cases}$$

- b) Determine the electric flux that passes through the surface defined by $Z=0$, $-a \leq x \leq a$, $-b \leq y \leq b$ (5 pts)

determine the electric flux that passes through the surface defined by $z = 0$, $-a \leq x \leq a$, $-b \leq y \leq b$: In the x - y plane, \mathbf{D} evaluates as the constant $\mathbf{D}(0) = 2d\rho_0 \mathbf{a}_z$. Therefore the flux passing through the given area will be

$$\Phi = \int_{-a}^a \int_{-b}^b 2d\rho_0 dx dy = \underline{8abd\rho_0} \text{ C}$$

- c) Determine the total charge contained within the region $-a \leq x \leq a$, $-b \leq y \leq b$, $-d \leq z \leq d$ (5 pts)

determine the total charge contained within the region $-a \leq x \leq a$, $-b \leq y \leq b$, $-d \leq z \leq d$: From part a, we have equal and opposite charge densities above and below the x - y plane. This means that within a region having equal volumes above and below the plane, the net charge is zero.

- d) Determine the total charge contained within the region $-a \leq x \leq a$, $-b \leq y \leq b$, $0 \leq z \leq 2d$ (5 pts)

determine the total charge contained within the region $-a \leq x \leq a$, $-b \leq y \leq b$, $0 \leq z \leq 2d$. In this case,

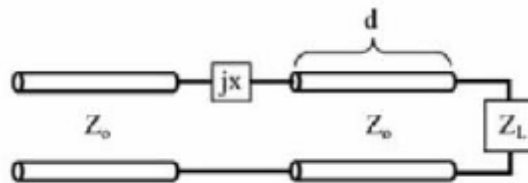
$$Q = -\rho_0 (2a) (2b) (2d) = \underline{-8abd\rho_0} \text{ C}$$

This is equivalent to the net *inward* flux of \mathbf{D} into the volume, as was found in part b.

Problem 2 (20 pts):

A matching network, using a reactive element in series with a length d of a transmission line, is to be used to match $35-j50 \Omega$ load to a 100Ω transmission line. Find the through line length d and the value of the reactive element for $F=1 \text{ GHz}$ if:

- a) a series capacitor is used. (10 pts)



First we normalize the load and locate it on the Smith Chart (point a, at $z_L = 0.35 - j0.5$, WTG = 0.419λ).

(a) need to move to point b, at $z = 1 + j1.4$, so that a capacitive element of value $jx = -j1.4$ can be added to provide an impedance match. Moving to this point b gives $d = 0.500\lambda + 0.173\lambda - 0.419\lambda = 0.254\lambda$. The capacitance is

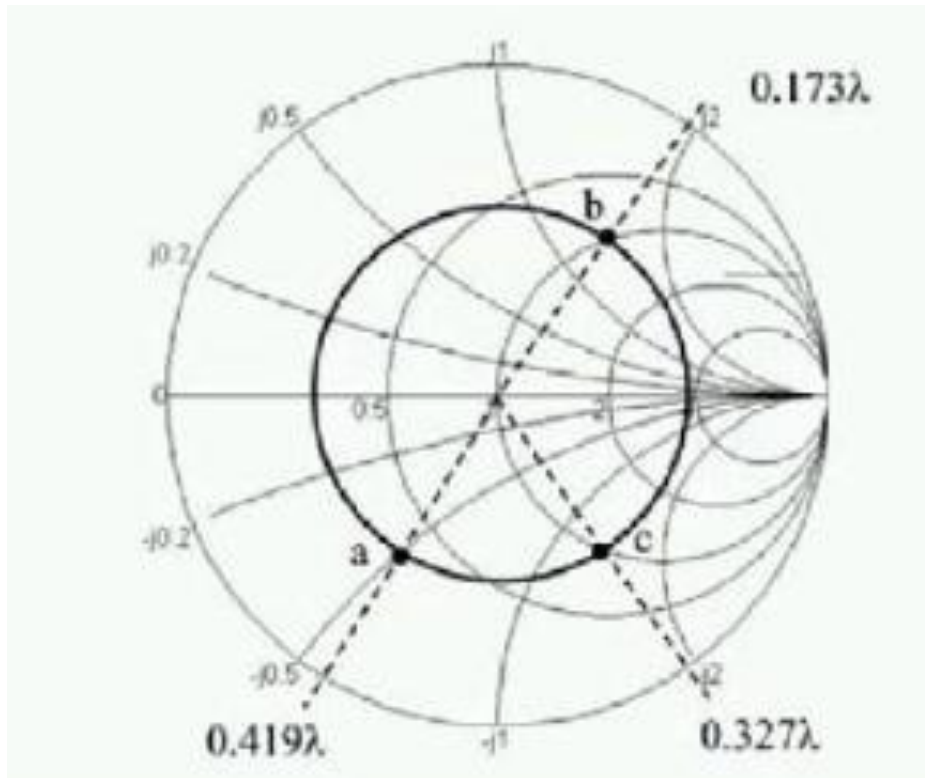
$$\frac{-j}{\omega C Z_o} = -j1.4,$$

$$C = \frac{1}{2\pi(1 \times 10^9)(100)(1.4)} = 1.14 \text{ pF}$$

b) If an inductor is used. (10 pts)

(b) Now we need to move to point c, at $z = 1 - j1.4$, so that an inductive element of value $jx = +j1.4$ can be added. Moving to this point c gives $d = 0.500\lambda + 0.327\lambda - 0.419\lambda = 0.408\lambda$. The inductance is

$$\frac{j\omega L}{Z_o} = j1.4, \quad L = \frac{(1.4)(100)}{2\pi(1 \times 10^9)} = 22.3 \text{ nH}$$



Problem 3 (20 pts):

A load impedance $Z_L = 200 + j160 \Omega$ is to be matched to a 100Ω line using a shorted shunt stub tuner. Find the solution that minimizes the length of the shorted stub.

Refer to Fig. P2.37a for the shunt stub circuit.

(1) Normalize the load (point a, $z_L = 2.0 + j1.6$).

(2) locate the normalized load admittance: y_L (point b)

(3) move from point b to point c, at the $y=1+jb$ circle ($0.500\lambda + 0.170\lambda - 0.458\lambda = 0.212\lambda$)

(4) move from the shorted end of the stub (normalized admittance point) to the point $y = 0 - jb$. ($\ell = 0.354 \lambda - 0.250 \lambda = 0.104 \lambda$.)

