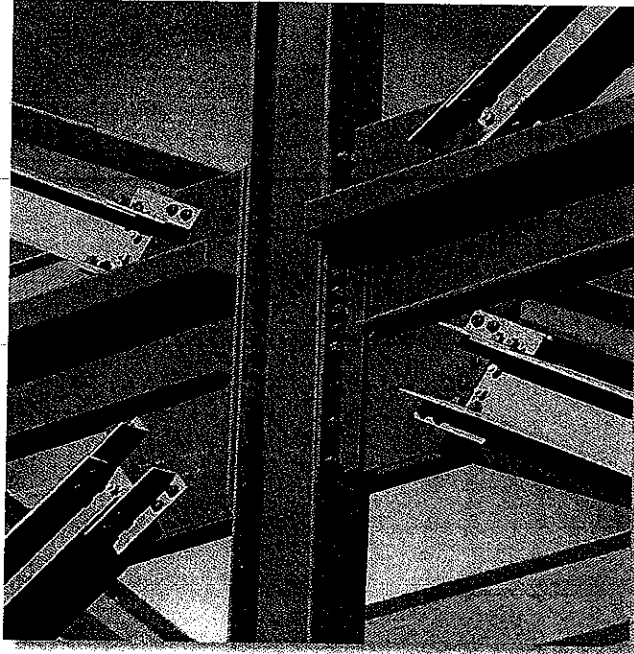


MECH 320-Mechanics of Materials
AMERICAN UNIVERSITY OF BEIRUT



STUDENT NAME:

ID:

Spring semester 2009-2010

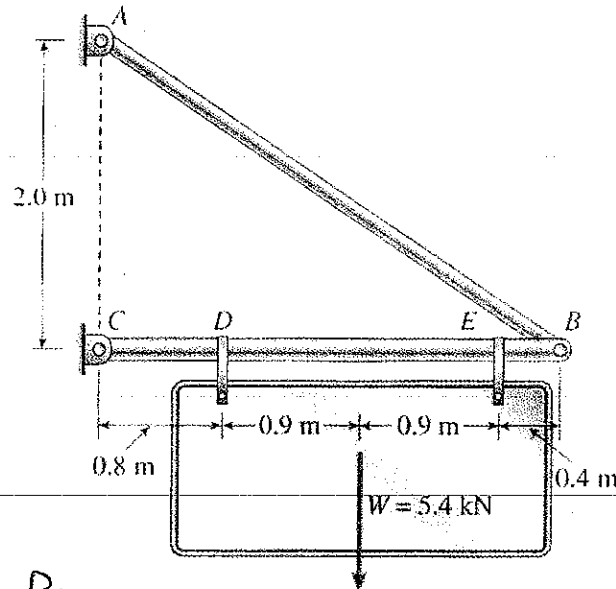
Instructors: Shehadeh M., and Nasser-Eddin M.

TIME ALLOWED: 2H

Problem 1. (25pts).

The two-bar truss ABC shown in the figure below has pin supports at points A and C, which are 2.0 m apart. Members AB and BC are steel bars, pin connected at joint B. The length of bar BC is 3.0 m. A sign weighing 5.4 kN is suspended from bar BC at points D and E, which are located 0.8 m and 0.4m, respectively, from the ends of the bar.

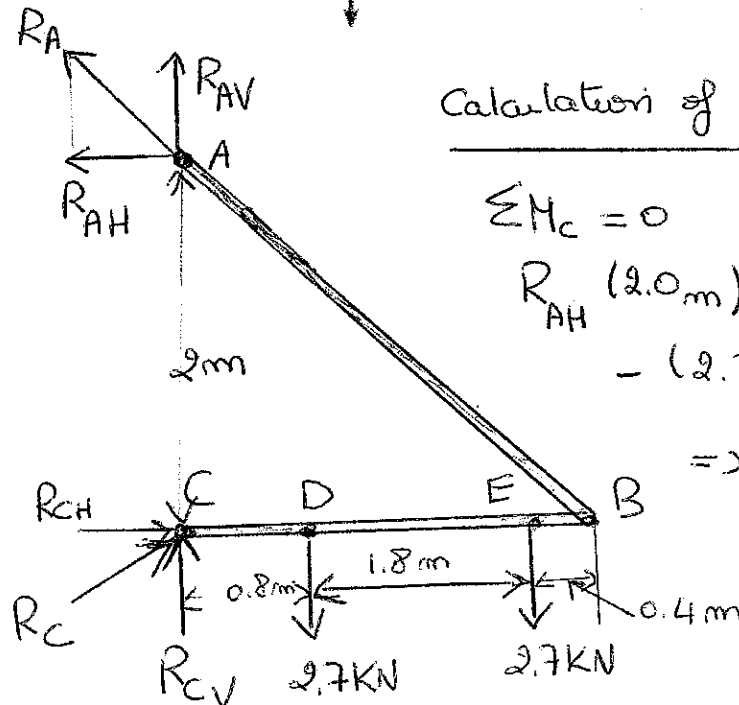
Determine the required cross sectional area of bar AB and the required diameter of the pin at support C if the allowable stresses in tension and shear are 125 MPa and 45 MPa, respectively. (Note: The pins at the supports are in double shear. Also, disregard the weights of members AB and BC).



Solution

1) Reactions
FBD

(fig a)

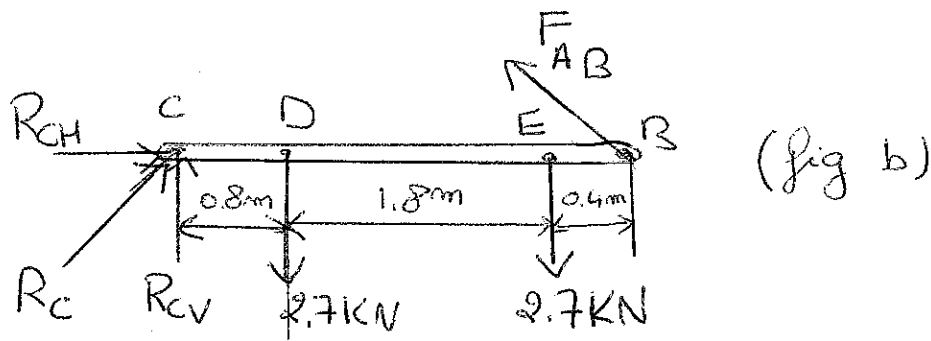


Calculation of R_{AH}

$$\sum M_c = 0$$

$$R_{AH} (2.0 \text{ m}) - (2.7 \text{ kN})(0.8 \text{ m}) - (2.7 \text{ kN})(2.6 \text{ m}) = 0$$

$$\Rightarrow R_{AH} = 4.6 \text{ kN}$$



Calculation of R_{CH} : $R_{CH} = R_{AH} = 4.6 \text{ kN}$

Calculation of R_{CV} and R_{AV} (fig b)

$$\sum M_B = 0 \quad -R_{CV}(3.0 \text{ m}) + (2.7 \text{ kN}) + (2.7 \text{ kN}) \times (0.4 \text{ m}) \times 2.2 \text{ m}$$

$$\Rightarrow R_{CV} = 2.34 \text{ kN}$$

fig (a): $\sum F_{\text{vert}} = 0$

$$R_{AV} + R_{CV} - 2.7 \text{ kN} - 2.7 \text{ kN} = 0$$

$$\Rightarrow R_{AV} = 3.060 \text{ kN}$$

calculation of R_A : $R_A = \sqrt{(R_{AH})^2 + (R_{AV})^2} = 5.516 \text{ kN}$

calculation of R_C : $R_C = \sqrt{(R_{CH})^2 + (R_{CV})^2} = 5.152 \text{ kN}$

Tensile force in bar AB: $F_{AB} = R_A = 5.516 \text{ kN}$

Shear force acting in pin C: $V_C = R_C = 5.152 \text{ kN}$

Required area of ~~bar~~ bar: $A_{AB} = \frac{F_{AB}}{\sigma_{\text{AIL}}} = \frac{5.516 \text{ kN}}{125 \text{ MPa}} = 44 \text{ mm}^2$

Required diameter of pin

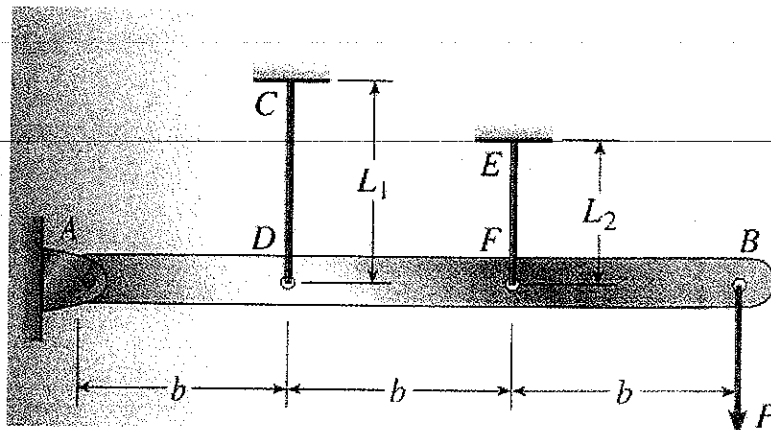
$$A_{\text{pin}} = \frac{V_C}{2\sigma_{\text{..}}} = \frac{5.152 \text{ kN}}{2(45 \text{ MPa})} = 57.2 \text{ mm}^2 \Rightarrow d_{\text{pin}} = \sqrt{\frac{4A_{\text{pin}}}{\pi}} = 8.54 \text{ mm}$$

Problem 2.(25 pts)

A horizontal rigid bar AB is pinned at end A and supported by two wires CD and EF at points D and F as shown in the figure below. A vertical load $P=1.5$ kN acts at end B of the bar. The bar has a length $=3b$. The wires CD and EF have length $L_1=0.40$ m and $L_2=0.30$ m. Also the wires CD and EF have diameters of 4 mm and 3mm respectively. The wire CD is made of aluminum with $E_{Al}=72$ GPa while the wire EF is made of Magnesium with $E_{Mg}=45$ GPa knowing that the allowable stresses in the Aluminum and Magnesium wires are 200 MPa and 175 MPa respectively

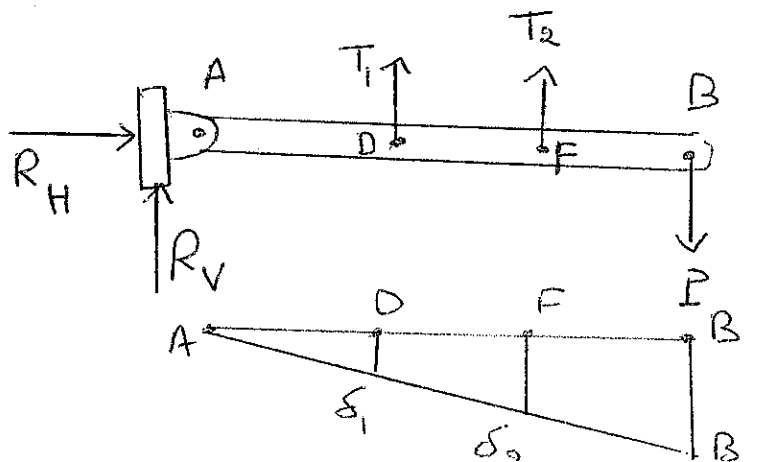
a- Calculate the normal stresses in bars EF and CD.

b- By reference to the values found in part a, determine if the materials used in the design are adequate.



Solution

Equilibrium



$$\sum M_A = 0$$

$$T_1 b + T_2 (2b) - P(3b) = 0 \Rightarrow T_1 + 2T_2 = 3P \quad (1)$$

Compatibility $AD = DF$

$$\delta_2 = 2\delta_1 \quad (2)$$

Force displacement relations

$$\delta_1 = \frac{T_1 L_1}{E_1 A_1} \quad \delta_2 = \frac{T_2 L_2}{E_2 A_2}$$

$$A_1 = \frac{\pi d_1^2}{4} \quad A_2 = \frac{\pi d_2^2}{4}$$

For simplicity: $f_1 = \frac{L_1}{E_1 A_1}$ $f_2 = \frac{L_2}{E_2 A_2}$

$$\Rightarrow \delta_1 = f_1 T_1 \quad \delta_2 = f_2 T_2 \quad (3, 4)$$

solution of equations

Substitute (3, 4) into (2) \Rightarrow

$$f_2 T_2 = 2 f_1 T_1 \quad (5)$$

Solving (5) and (1) each containing T_1 & T_2 -

$$T_1 = \frac{3 f_2 P}{4 f_1 + f_2} \quad T_2 = \frac{6 f_1 P}{4 f_1 + f_2}$$

Normal stresses

$$\sigma_1 = \frac{T_1}{A_1} = \frac{3P}{A_1} \left(\frac{f_2}{4f_1 + f_2} \right)$$

$$f_1 = \frac{L_1}{A_1 E_1} = 0.4420 \times 10^{-6} \text{ m/N} ;$$

$$f_2 = \frac{L_2}{E_2 A_2} = 0.9431 \times 10^{-6} \text{ m/N} ;$$

$$P = 1.5 \times 10^3 \text{ N} ; A_1 = \frac{\pi d_1^2}{4} = 12.57 \text{ mm}^2$$

$$\Rightarrow \sigma_1 = \frac{3 \times 1.5 \times 10^3}{12.57 \times 10^{-6}} \left(\frac{0.9431 \times 10^{-6}}{4 \times 0.442 \times 10^{-6} + 0.9431 \times 10^{-6}} \right)$$

$$= 124.44 \text{ MPa}$$

$$\sigma_2 = \frac{6P}{A_2} \left(\frac{f_1}{4f_1 + f_2} \right) = \frac{6 \times 1.5 \times 10^3}{7.069 \times 10^{-6}} \left(\frac{0.4420}{4 \times 0.442 + 0.9431} \right)$$

$$= 1,277,777 \text{ MPa}$$

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Material 1 \rightarrow Acceptable

because $\sigma_1 < \sigma_{All}$

Material 2 \rightarrow Non acceptable

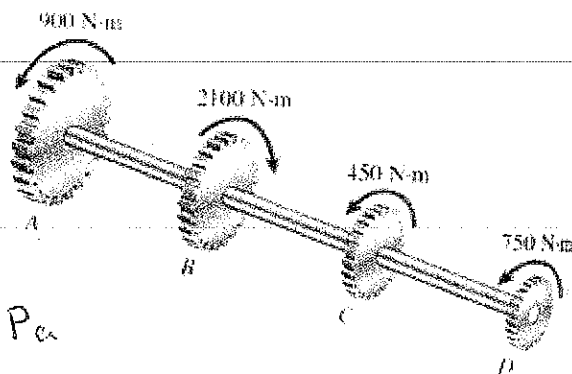
because $\sigma_2 > \sigma_{All}$

change it to a stronger material.

Problem 3. (25 pts)

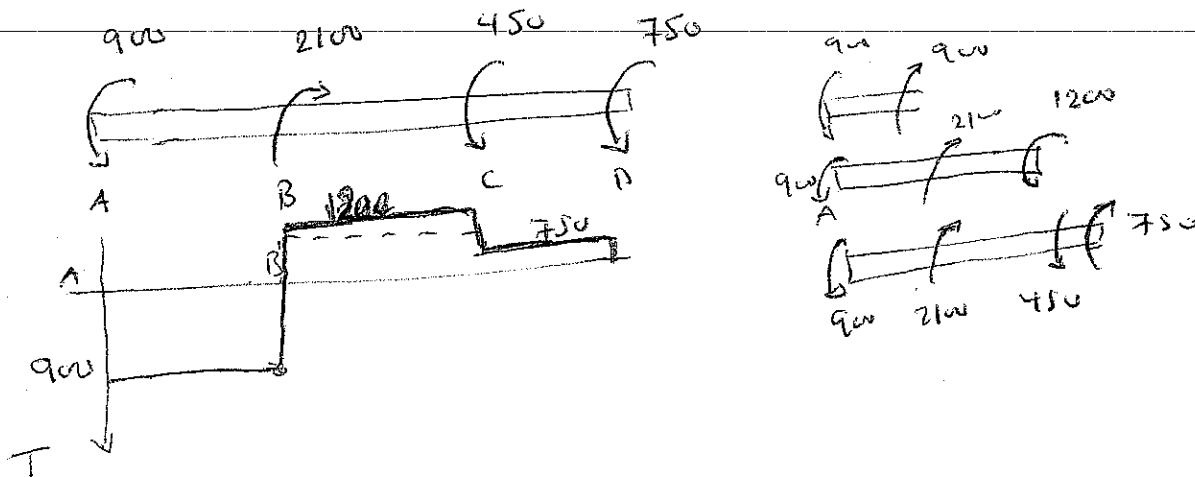
Four gears are attached to a circular shaft and transmit the torques shown in the figure below. The Allowable shear stress in the shaft is 70 MPa.

- a- What is the required diameter d of the shaft if it has a solid cross-section?
- b- Another design is suggested such that a hollow shaft of an inside diameter of 40 mm and an outside diameter of 60 mm is used, would the shaft sustain the applied torque? Justify your answer.



$\tau_{\text{all}} = 70 \text{ MPa}$

Draw the torque diagram



From the torque diagram, the maximum torque is applied in the section BC and that is where the maximum stress will be induced.

(a)

$$\tau = \frac{T r}{J}$$

$$\tau_{max} = \frac{16 T}{\pi d^3} = \frac{16 \times (1200)}{\pi \times \cancel{d^3}} = 70 \times 10^6$$

$$\tau_{max} = \frac{16 T}{\pi d^3} \quad \Rightarrow \quad \cancel{d^3} = \frac{16 T}{\pi \tau_{max}}$$

$$d = \left(\frac{16 T}{\pi \tau_{max}} \right)^{1/3} = \frac{16 \times 1200}{\pi \times 70 \times 10^6}$$

$$d = \left(\frac{16 \times 1200}{\pi \times 70 \times 10^6} \right)^{1/3} = 0.0443 \text{ m}$$

$$\therefore d = 44.3 \text{ mm}$$

(b) $d_i = 40 \text{ mm}$ $d_o = 60 \text{ mm}$

$$\tau = \frac{T r}{J}, \quad J = \frac{\pi}{32} (d_o^4 - d_i^4) = \frac{\pi}{32} (60^4 - 40^4) \times 10^{-12} \text{ m}^4$$

$$\therefore J = 1.021 \times 10^{-6} \text{ mm}^4$$

$$r = 30 \times 10^{-3}$$

$$\therefore \tau = \frac{1200 \times 30 \times 10^{-3}}{1.021 \times 10^{-6}} = 35.26 \text{ MPa}$$

The shaft would sustain the applied torque because $\tau_{max} < \tau_{all}$.

$$\delta_D = \frac{20 \times 0.7}{E_{st} A_{st}} + \frac{20 \times 0.5}{E_{al} A_{al}} + \frac{12 \times 0.3}{E_{al} A_{al}}$$

$$A_{st} = \frac{\pi}{4} (10 \times 10^{-3})^2 = 78.54 \times 10^{-6} \text{ m}^2$$

$$A_{al} = \frac{\pi}{4} (30 \times 10^{-3})^2 = 706.86 \times 10^{-6} \text{ m}^2$$

$$\therefore \delta_D = \frac{20 \times 0.7 \times 1000}{200 \times 10^9 \times 78.54 \times 10^{-6}} + \frac{20 \times 0.5 \times 1000}{70 \times 10^9 \times 706.86 \times 10^{-6}} + \frac{12 \times 0.3 \times 1000}{70 \times 10^9 \times 706.86 \times 10^{-6}}$$

$$\therefore \delta_D = 0.000891 + 0.000202 + 0.00072762$$

$$\delta_D \approx 0.00165 \text{ m} = 1.65 \text{ mm}$$

b- Maximum stress \Rightarrow since the steel rod has smaller cross section and the maximum load is applied on it then the max stress will be induced there.

$$\sigma_{max} = \frac{P}{A}$$

$$\sigma_{max} = \frac{20 \times 10^3}{\frac{\pi}{4} (10 \times 10^{-3})^2} = 254.65 \text{ MPa.}$$

$$c - \sigma_{st} = E \epsilon_{st} \Rightarrow \epsilon = \frac{\sigma}{E} = \frac{254.65}{200 \times 10^9} = 1.273 \times 10^{-3}$$

$$\nu = - \frac{\epsilon_{al}}{\epsilon_{st}} \Rightarrow \epsilon_{al} = - \nu_{st} \epsilon_{max} = -(0.3)(1.273) \times 10^{-3}$$

$$\therefore \epsilon_{al} = -0.382 \times 10^{-3} = \frac{\delta_D}{D}$$

$$\therefore \delta_D = (-0.382 \times 10^{-3})(10 \text{ mm}) = -3.82 \times 10^{-3} \text{ mm}$$