

Example B-9-5

Referring to the closed-loop system shown in Figure 9-63, design a lead compensator $G_c(s)$ such that the phase margin is 45° , gain margin is not less than 8 dB, and the static velocity error constant K_v is 4.0 sec^{-1} . Plot unit-step and unit-ramp response curves of the compensated system with LabVIEW.

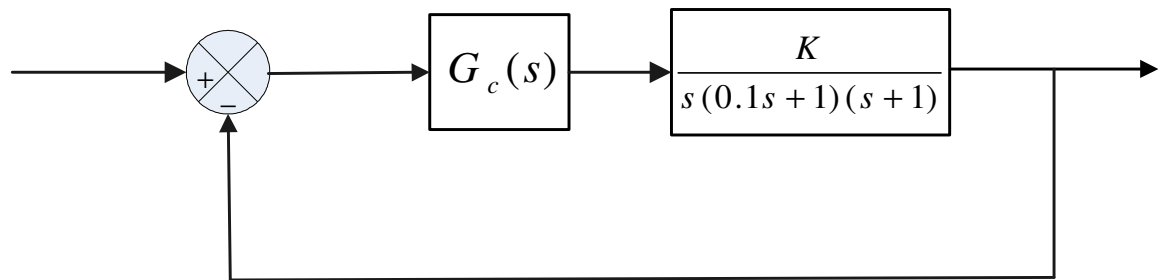


Figure 9-63. Closed-loop system

Solution. Let us use the lead compensator

$$G_c(s) = K_c \alpha \frac{T s + 1}{\alpha T s + 1} = K_c \frac{s + \frac{1}{T}}{s + \frac{1}{\alpha T}}$$

Since K_v is specified as 4.0 sec^{-1} , we have

$$K_v = \lim_{s \rightarrow 0} s K_c \alpha \frac{T s + 1}{\alpha T s + 1} \frac{K}{s(0.1s + 1)(s + 1)} = K_c \alpha K = 4$$

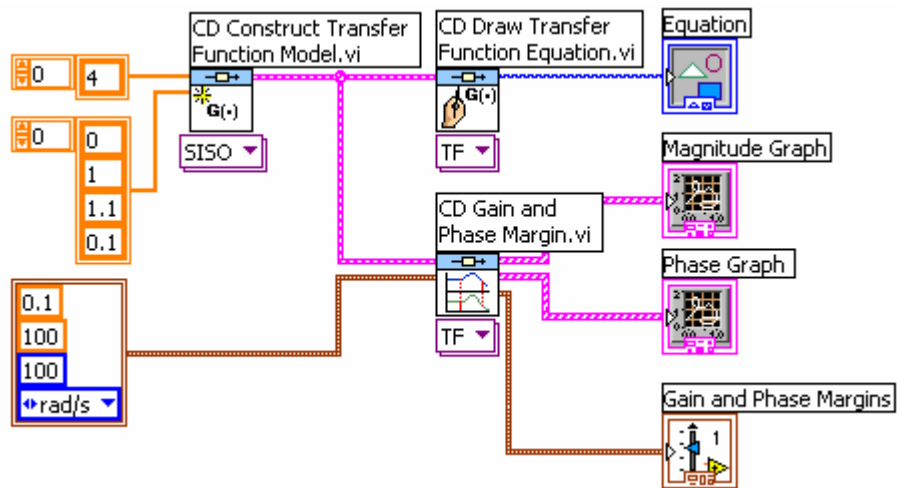
Let us set $K = 1$ and define $K_c \alpha = \hat{K}$. Then

$$\hat{K} = 4$$

Next, plot a Bode diagram of

$$\frac{4}{s(0.1s + 1)(s + 1)} = \frac{4}{0.1s^3 + 1.1s^2 + s}$$

LabVIEW Program B-9-5(a) produces the Bode diagram shown in Figure 9-63(a).



LabVIEW Program B-9-5(a)

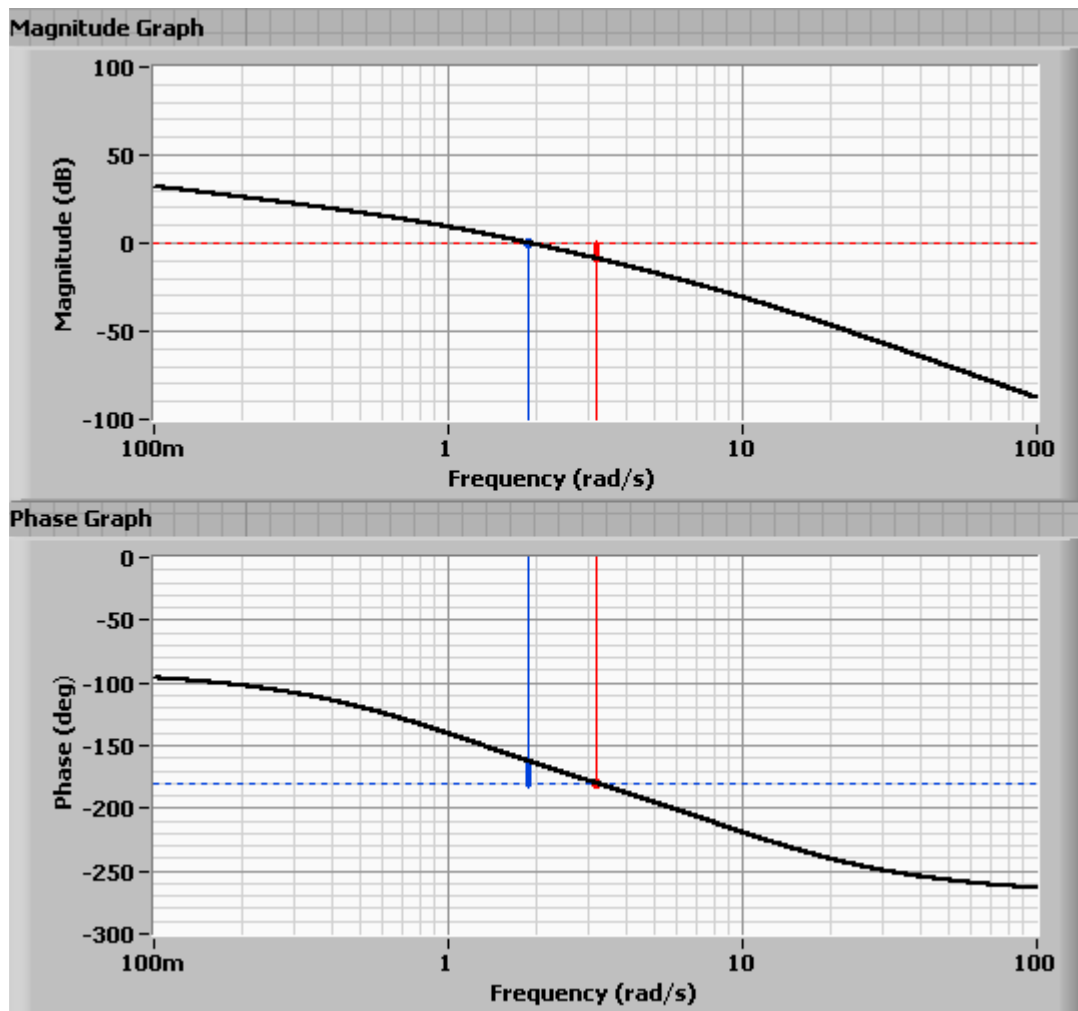


Figure 9-63(a). Bode plot of $G(s) = [s(0.1s+1)(s+1)]$

From this plot, the phase and gain margins are 17° and 8.7 dB, respectively.

Since the specifications call for a phase margin of 45° , let us choose

$$\phi_m = 45^\circ - 17^\circ + 12^\circ = 40^\circ$$

(This means that 12° has been added to compensate for the shift in the gain crossover frequency.) The maximum phase lead is 40° . Since

$$\sin \phi_m = \frac{1 - \alpha}{1 + \alpha} \quad (\phi_m = 40^\circ)$$

α is determined as 0.2174. Let us choose, instead of 0.2174, α to be 0.21, or

$$\alpha = 0.21$$

Next step is to determine the corner frequencies $\omega = 1/T$ and $\omega = 1/(\alpha T)$ of the lead compensator. Note that the maximum phase-lead angle ϕ_m occurs at the geometric mean of the two corner frequencies, or $\omega = 1/(\sqrt{\alpha T})$. The amount of the modification in the magnitude curve at $\omega = 1/(\sqrt{\alpha T})$ due to the inclusion of the term $(Ts+1)/(\alpha Ts+1)$ is

$$\left| \frac{1 + j\omega T}{1 + j\omega \alpha T} \right|_{\omega=1/(\sqrt{\alpha T})} = \frac{1}{\sqrt{\alpha}}$$

Note that

$$\frac{1}{\sqrt{\alpha}} = \frac{1}{\sqrt{0.21}} = 6.7778 \text{ dB}.$$

We need to find the frequency point where, when the lead compensator is added, the total magnitude becomes 0 dB. The magnitude of $G(j\omega)$ is -6.7778 dB corresponds to $\omega = 2.81$ rad/sec. We select this frequency to be the new gain crossover frequency ω_c . Then we obtain

$$\frac{1}{T} = \sqrt{\alpha} \omega_c = \sqrt{0.21} \times 2.81 = 1.2877$$

$$\frac{1}{\alpha T} = \frac{\omega_c}{\sqrt{\alpha}} = \frac{2.81}{\sqrt{0.21}} = 6.1319$$

Hence

$$G_c(s) = K_c \frac{s + 1.2877}{s + 6.1319}$$

and

$$K_c = \frac{\hat{K}}{\alpha} = \frac{4}{0.21}$$

Thus

$$G_c(s) = \frac{4}{0.21} \frac{s+1.2877}{s+6.1319} = 4 \frac{0.7766s+1}{0.16308s+1}$$

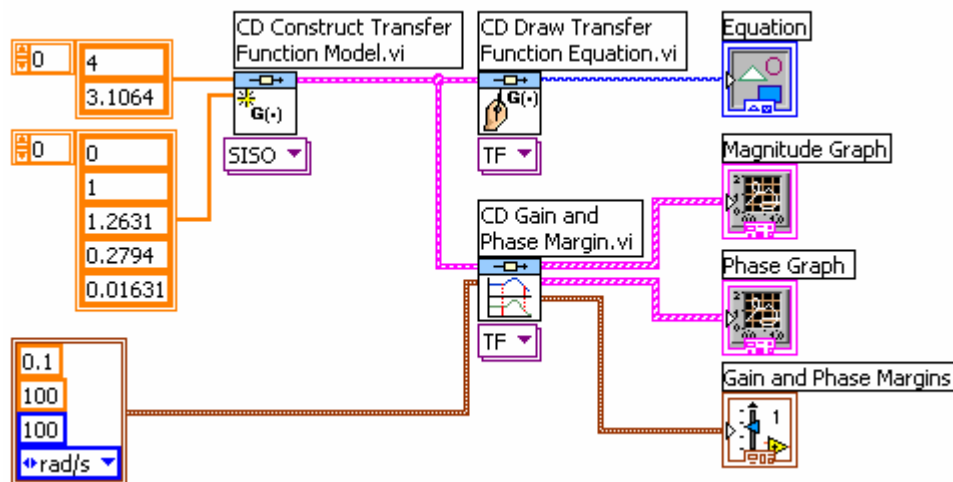
The open-loop transfer function becomes as

$$\begin{aligned} G_c(s)G(s) &= 4 \frac{0.7766s+1}{0.16308s+1} \frac{1}{s(0.1s+1)(s+1)} \\ &= \frac{3.1064s+4}{0.01631s^4 + 0.2794s^3 + 1.2631s^2 + s} \end{aligned}$$

the closed-loop transfer function is

$$\frac{C(s)}{R(s)} = \frac{3.1064s+4}{0.01631s^4 + 0.2794s^3 + 1.2631s^2 + 4.1064s+4}$$

LabVIEW Program B-9-5(b) produces the Bode plots of the closed-loop transfer function as shown in Figure 9-63(b).



LabVIEW Program B-9-5(b)

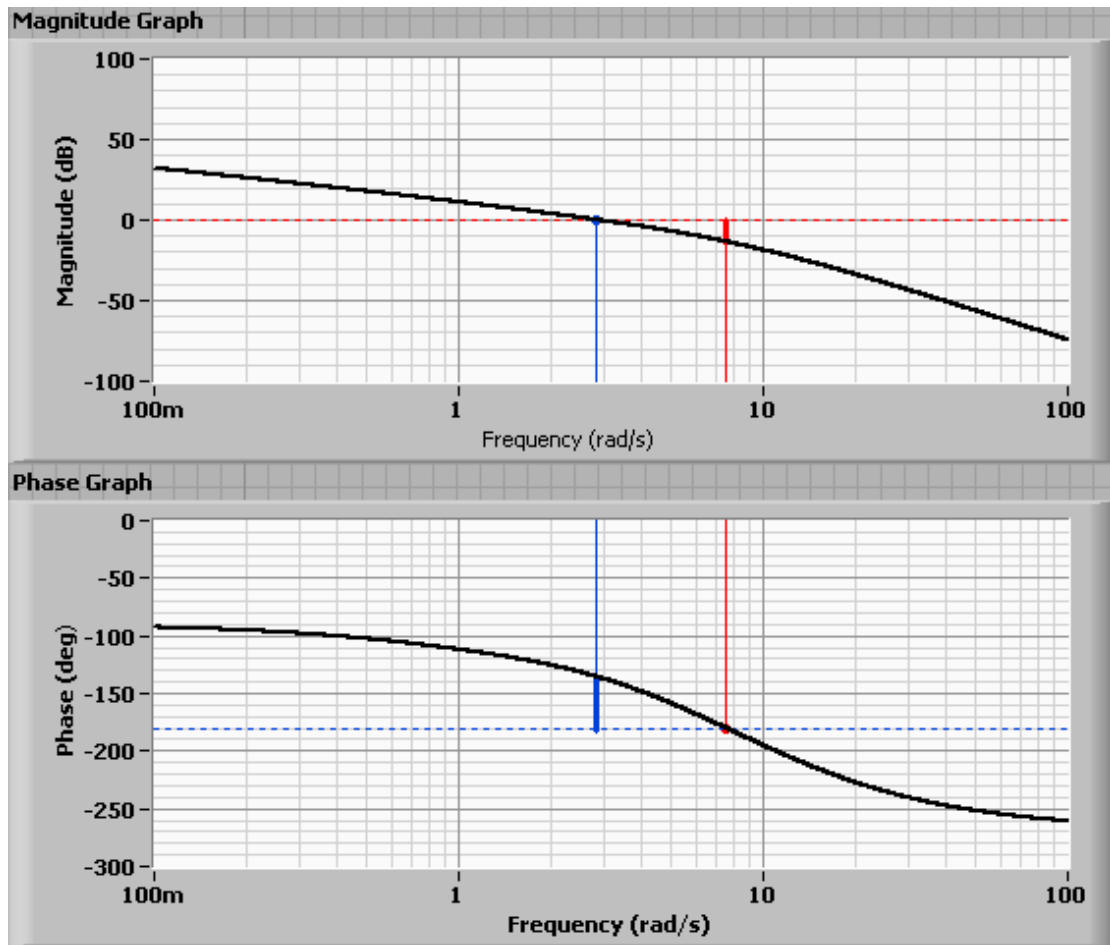
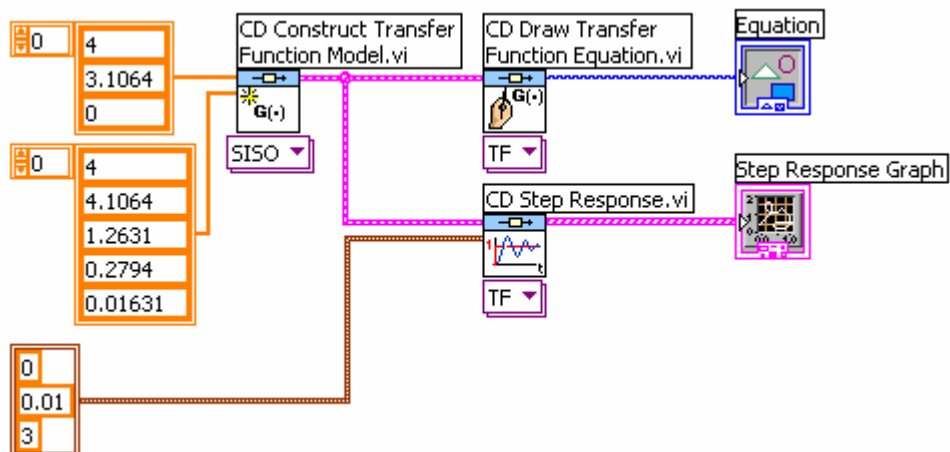


Figure 9-63(b). Bode Diagram of the closed-loop system

LabVIEW Program B-9-5(c) produces the unit-step response curve as shown in Figure 9-63(c).



LabVIEW Program B-9-5(c)

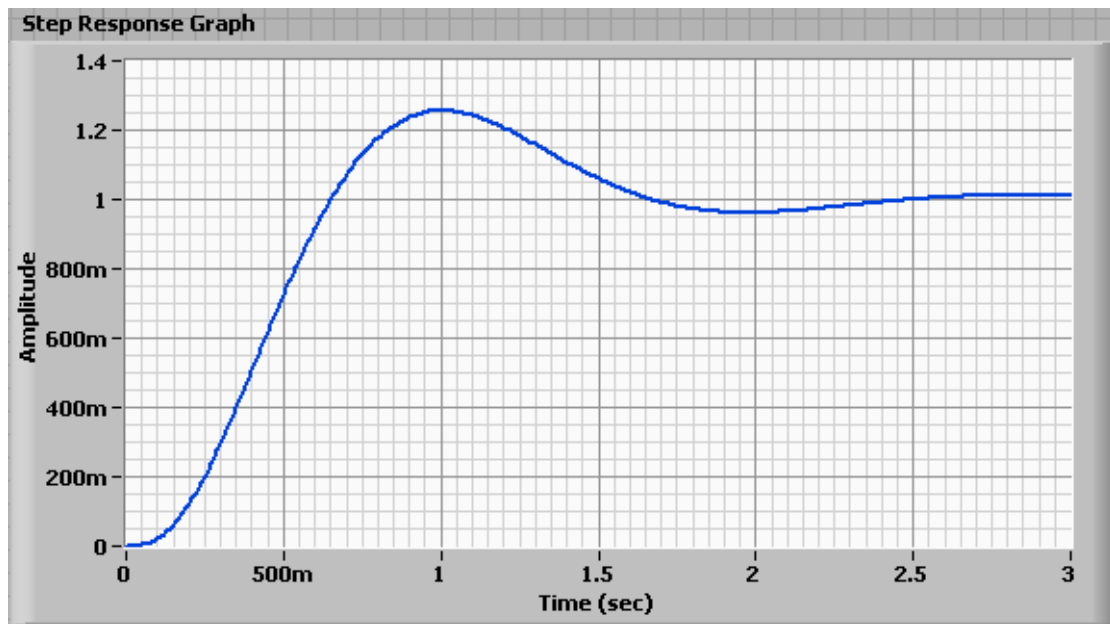
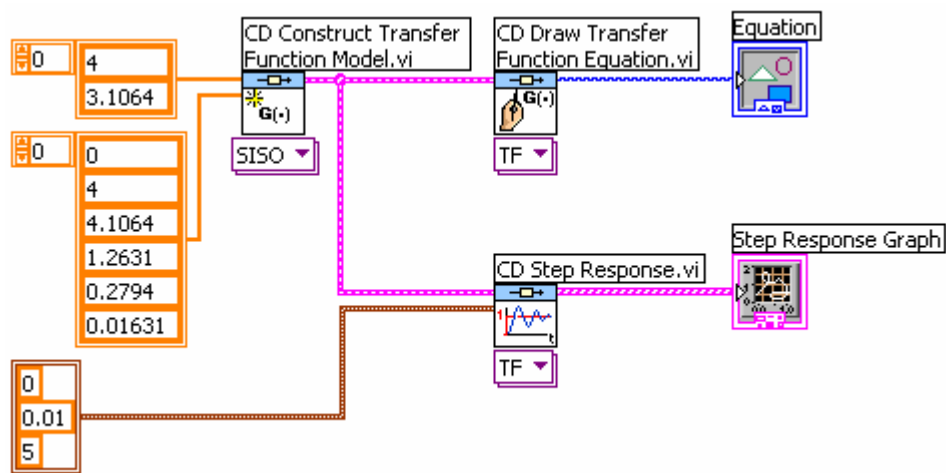


Figure 9-63(c). Unit-step response curve

Similarly, LabVIEW Program B-9-5(d) produces the unit-ramp response curve as shown in Figure 9-63(d).



LabVIEW Program B-9-5(d)

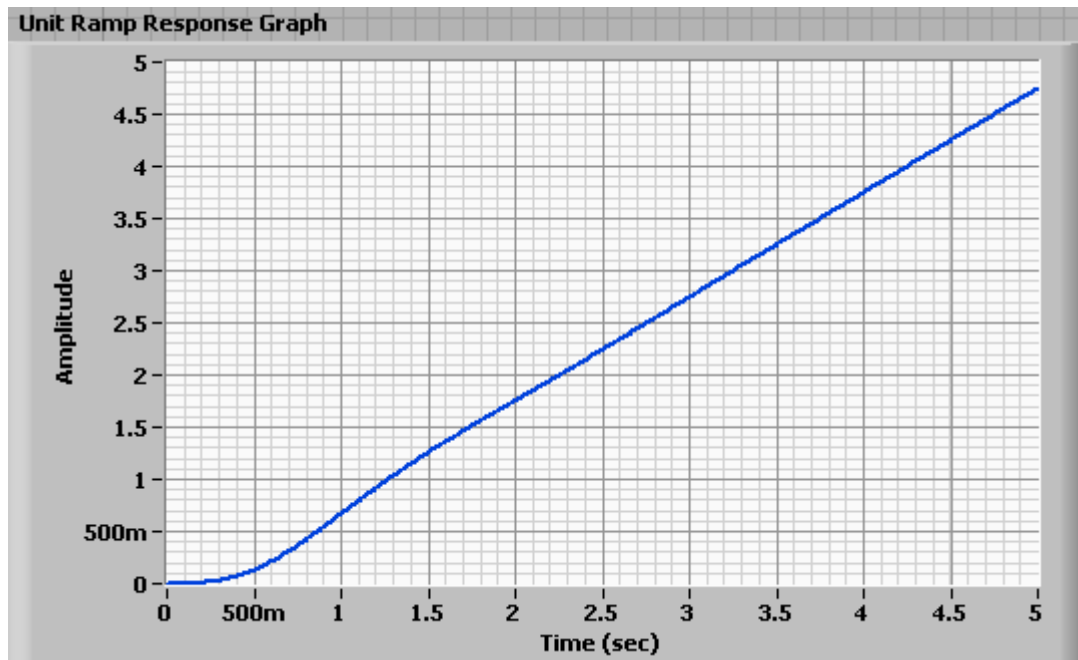


Figure 9-63(d). Unit-ramp response curve