

Homework # 9 Solution (Exercises 12.3, 8, 11 & 14)

B-12-3. Referring to Equation (12-18), the state-feedback gain matrix K can be given by

$$K = [0 \ 0 \ 1] \begin{bmatrix} B & AB & A^2B \end{bmatrix}^{-1} \phi(A)$$

where

$$\phi(A) = A^3 + \alpha_1 A^2 + \alpha_2 A + \alpha_3 I$$

The values of α_1 , α_2 , and α_3 are determined from the desired characteristic equation:

$$\begin{aligned} |sI - (A - BK)| &= (s + 2 + j4)(s + 2 - j4)(s + 10) \\ &= s^3 + 14s^2 + 60s + 200 \\ &= s^3 + \alpha_1 s^2 + \alpha_2 s + \alpha_3 \end{aligned}$$

Thus,

$$\alpha_1 = 14, \quad \alpha_2 = 60, \quad \alpha_3 = 200$$

Then

$$\phi(A) = \begin{bmatrix} 0 & 1 & 0 \\ 0 & 0 & 1 \\ -1 & -5 & -6 \end{bmatrix}^3 + 14 \begin{bmatrix} 0 & 1 & 0 \\ 0 & 0 & 1 \\ -1 & -5 & -6 \end{bmatrix}^2 + 60 \begin{bmatrix} 0 & 1 & 0 \\ 0 & 0 & 1 \\ -1 & -5 & -6 \end{bmatrix} + 200 \begin{bmatrix} 1 & 0 & 0 \\ 0 & 1 & 0 \\ 0 & 0 & 1 \end{bmatrix}$$

$$= \begin{bmatrix} 199 & 55 & 8 \\ -8 & 159 & 7 \\ -7 & -43 & 117 \end{bmatrix}$$

Since

$$\begin{bmatrix} B & AB & A^2B \\ \text{m} & \text{mm} & \text{mm} \end{bmatrix} = \begin{bmatrix} 0 & 1 & 1 \\ 1 & 1 & -11 \\ 1 & -11 & 60 \end{bmatrix}$$

we have the desired state-feedback gain matrix K as follows:

$$\begin{aligned} K &= [0 \ 0 \ 1] \begin{bmatrix} 0 & 1 & 1 \\ 1 & 1 & -11 \\ 1 & -11 & 60 \end{bmatrix}^{-1} \begin{bmatrix} 199 & 55 & 8 \\ -8 & 159 & 7 \\ -7 & -43 & 117 \end{bmatrix} \\ &= [0 \ 0 \ 1] \begin{bmatrix} 0.7349 & 0.8554 & 0.1446 \\ 0.8554 & 0.0120 & -0.0120 \\ 0.1446 & -0.0120 & 0.0120 \end{bmatrix} \\ &\quad \times \begin{bmatrix} 199 & 55 & 8 \\ -8 & 159 & 7 \\ -7 & -43 & 117 \end{bmatrix} \\ &= [0 \ 0 \ 1] \begin{bmatrix} 138.3976 & 170.2169 & 28.7831 \\ 170.2169 & 49.4819 & 5.5181 \\ 28.7831 & 5.5181 & 2.4819 \end{bmatrix} \\ &= [28.7831 \quad 5.5181 \quad 2.4819] \end{aligned}$$

B-12-8. From Figure 12-49 we obtain

$$u = k_1(r - x_1) - k_2 x_2 - k_3 x_3 = -\underset{mm}{K}x + k_1 r$$

where

$$\underset{m}{K} = [k_1 \quad k_2 \quad k_3]$$

Noting that the rank of

$$\underset{m}{M} = \begin{bmatrix} \underset{m}{B} & \underset{mm}{AB} & \underset{mm}{A^2B} \end{bmatrix} = \begin{bmatrix} 0 & 0 & 1 \\ 0 & 1 & -6 \\ 1 & -6 & 31 \end{bmatrix}$$

is three, arbitrary pole placement is possible. The characteristic equation for this system is

$$\begin{aligned} |sI - \underset{m}{A}| &= \begin{vmatrix} s & -1 & 0 \\ 0 & s & -1 \\ 0 & 5 & s+6 \end{vmatrix} = s^3 + 6s^2 + 5s \\ &= s^3 + a_1 s^2 + a_2 s + a_3 = 0 \end{aligned}$$

Hence

$$a_1 = 6, \quad a_2 = 5, \quad a_3 = 0$$

Since the state equation for the system is already in the controllable canonical form, we have $\underset{m}{T} = \underset{m}{I}$. The desired characteristic equation is

$$\begin{aligned} (s + 2 + j4)(s + 2 - j4)(s + 10) &= s^3 + 14s^2 + 60s + 200 \\ &= s^3 + \alpha_1 s^2 + \alpha_2 s + \alpha_3 \end{aligned}$$

from which we obtain

$$\alpha_1 = 14, \quad \alpha_2 = 60, \quad \alpha_3 = 200$$

Then

$$\begin{aligned} K_m &= [\alpha_3 - a_3 \quad \alpha_2 - a_2 \quad \alpha_1 - a_1] T_m^{-1} \\ &= [200 - 0 \quad 60 - 5 \quad 14 - 6] I_m \\ &= [200 \quad 55 \quad 8] \end{aligned}$$

The state equation for the designed system is

$$\begin{aligned} \dot{x}_m &= A_m x_m + B_m u = A_m x_m + B_m (-K_m x_m + k_1 r) \\ &= (A_m - B_m K_m) x_m + B_m k_1 r \end{aligned}$$

Since

$$A_m - B_m K_m = \begin{bmatrix} 0 & 1 & 0 \\ 0 & 0 & 1 \\ 0 & -5 & -6 \end{bmatrix} - \begin{bmatrix} 0 \\ 0 \\ 1 \end{bmatrix} [200 \quad 55 \quad 8] = \begin{bmatrix} 0 & 1 & 0 \\ 0 & 0 & 1 \\ -200 & -60 & -14 \end{bmatrix}$$

we have

$$\begin{bmatrix} \dot{x}_1 \\ \dot{x}_2 \\ \dot{x}_3 \end{bmatrix} = \begin{bmatrix} 0 & 1 & 0 \\ 0 & 0 & 1 \\ -200 & -60 & -14 \end{bmatrix} \begin{bmatrix} x_1 \\ x_2 \\ x_3 \end{bmatrix} + \begin{bmatrix} 0 \\ 0 \\ 200 \end{bmatrix} r \quad (1)$$

The output equation is

$$y = [1 \quad 0 \quad 0] \begin{bmatrix} x_1 \\ x_2 \\ x_3 \end{bmatrix} \quad (2)$$

The unit-step response of the designed system can be obtained from Equations (1) and (2) by substituting $r = 1(t)$ and finding $y(t)$. A MATLAB program to obtain the unit-step response curve [$y(t)$ versus t curve] is given on the next page.

```
>> A = [0 1 0; 0 0 1; -200 -60 -14]
```

```
A =
```

```
    0    1    0
    0    0    1
   -200   -60  -14
```

```
>> B = [0; 0; 200]
```

```
B =
```

```
    0
    0
   200
```

```
>> C = [1 0 0]
```

```
C =
```

```
    1    0    0
```

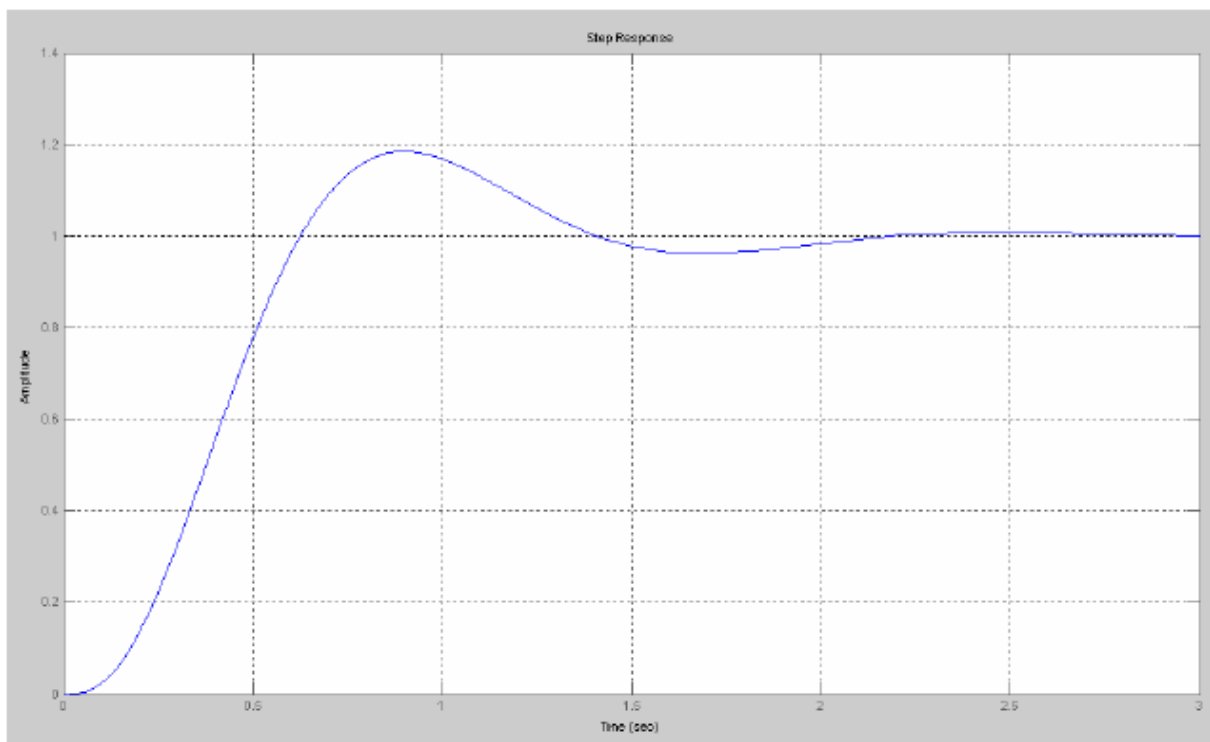
```
>> D=[0]
```

```
D =
```

```
    0
```

```
>> step(A,B,C,D)
```

```
>> grid
```



B-12-11. A full-order state observer for the given system is designed by use of MATLAB. The MATLAB program used for the design of the state observer is given below.

```

% ***** Design of full-order state observer *****
A=[0 1 0;0 0 1;-5 -6 0];
C=[1 0 0];
L=[-10 -10 -15];
Ke=acker(A',C',L)
Warning: Pole locations are more than 10% in error.

Ke =

    35
   394
  1285

```

Referring to Equation (12-60), the full-order state observer is given by

$$\dot{\tilde{x}} = (A - K_e C) \tilde{x} + B u + K_e y$$

$$\begin{bmatrix} \dot{\tilde{x}}_1 \\ \dot{\tilde{x}}_2 \\ \dot{\tilde{x}}_3 \end{bmatrix} = \begin{bmatrix} -35 & 1 & 0 \\ -394 & 0 & 1 \\ -1290 & -6 & 0 \end{bmatrix} \begin{bmatrix} \tilde{x}_1 \\ \tilde{x}_2 \\ \tilde{x}_3 \end{bmatrix} + \begin{bmatrix} 0 \\ 0 \\ 1 \end{bmatrix} u + \begin{bmatrix} 35 \\ 394 \\ 1285 \end{bmatrix} y$$

B-12-14. We shall use the MATLAB approach to solve this problem. The first MATLAB program given in the next page determines the state feedback gain matrix K and the observer gain matrix K_e . The observer to be designed is a full-order observer.

```

% **** Determination of K and Ke ****
A=[0 1 0;0 0 1;-6 -11 -6];
B=[0;0;1];
C=[1 0 0];
J=[-1+j -1-j -5];
K=acker(A,B,J)

K =

    4    1    1

L=[-6 -6 -6];
Ke=acker(A',C',L)

Ke =

    12
    25
   -72

```

The state feedback gain matrix K and the observer gain matrix K_e thus obtained are as follows:

$$K = \begin{bmatrix} 4 & 1 & 1 \end{bmatrix}$$

$$K_e = \begin{bmatrix} 12 \\ 25 \\ -72 \end{bmatrix}$$

The second MATLAB program given below determines the transfer function of the observer controller.

```

% Obtaining transfer function of observer controller — full-order observer
A=[0 1 0;0 0 1;-6 -11 -6];
B=[0;0;1];
C=[1 0 0];
K=[4 1 1];
Ke=[12;25;-72];
AA=A-Ke*C-B*K;
BB=Ke;
CC=K;
DD=0;
[num,den]=ss2tf(AA,BB,CC,DD)

num =

    0    1.0000   119.0000   618.0000

den =

    1.0000   19.0000   121.0000   257.0000

```

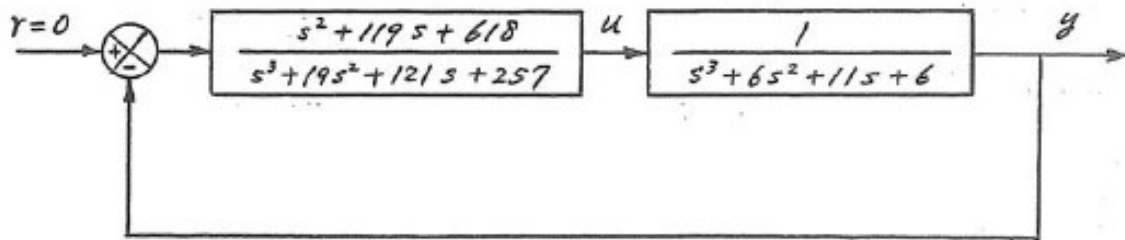
The transfer function of the observer controller is

$$\frac{U(s)}{-Y(s)} = \frac{s^2 + 119s + 618}{s^3 + 19s^2 + 121s + 257}$$

The transfer function of the given system in state space form is

$$G(s) = \frac{1}{s^3 + 6s^2 + 11s + 6}$$

A block diagram of the designed system is shown below.



Notice that the designed system is of sixth order.