

**QUIZ 2**  
**Spring 2003-2004**  
 (Thursday, May 13, 2004)  
**CIVE 311 – STRUCTURES I**  
**CLOSED BOOK, 1 HOUR & 45 MN**

Name: SOLTUON ID#: 2

**NOTES**

- 2 PROBLEMS – 13 PAGES.
- ALL YOUR ANSWERS SHOULD BE PROVIDED ON THE QUESTION SHEETS.
- **TWO EXTRA SHEETS ARE PROVIDED AT THE END**
- **ASK FOR ADDITIONAL SHEETS IF YOU NEED MORE SPACE**
- SOME ANSWERS MAY REQUIRE MUCH LESS THAN THE SPACE PROVIDED.
- **DO NOT USE THE BACK OF THE SHEETS FOR ANSWERS.**
- DRAFT BOOKLET WILL BE PROVIDED; BUT DO NOT USE FOR ANSWERS.
- BOTH QUESTION SHEETS AND DRAFT BOOKLET SHOULD BE RETURNED.
- CHECK BOXES ARE FOR YOU TO CONFIRM THAT HAVE SOLVED A QUESTION

**YOUR COMMENT(S)**

Some tough calculations.

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**DO NOT WRITE IN THE SPACE BELOW**

**MY COMMENT(S)**

Symmetry makes it easier

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**YOUR GRADE**

Problem I: 65 /65  
 Problem II: 35 /35  
 Other: . . . . .

**TOTAL:** 100 /100

**Problem I: (65 points)**

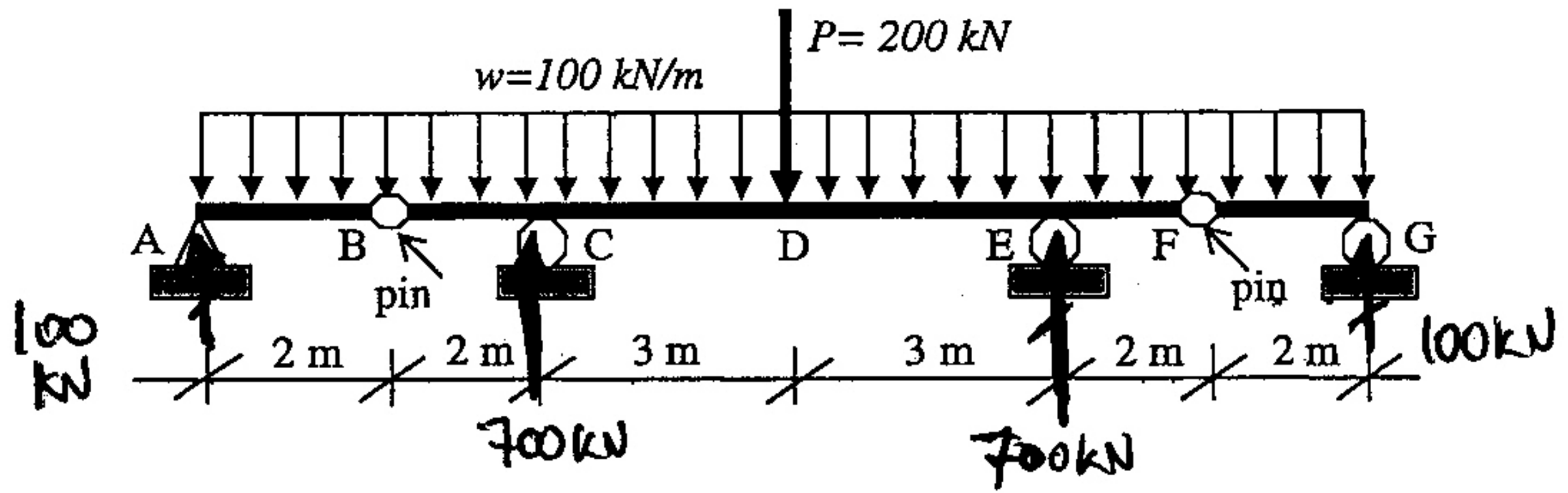


Figure I

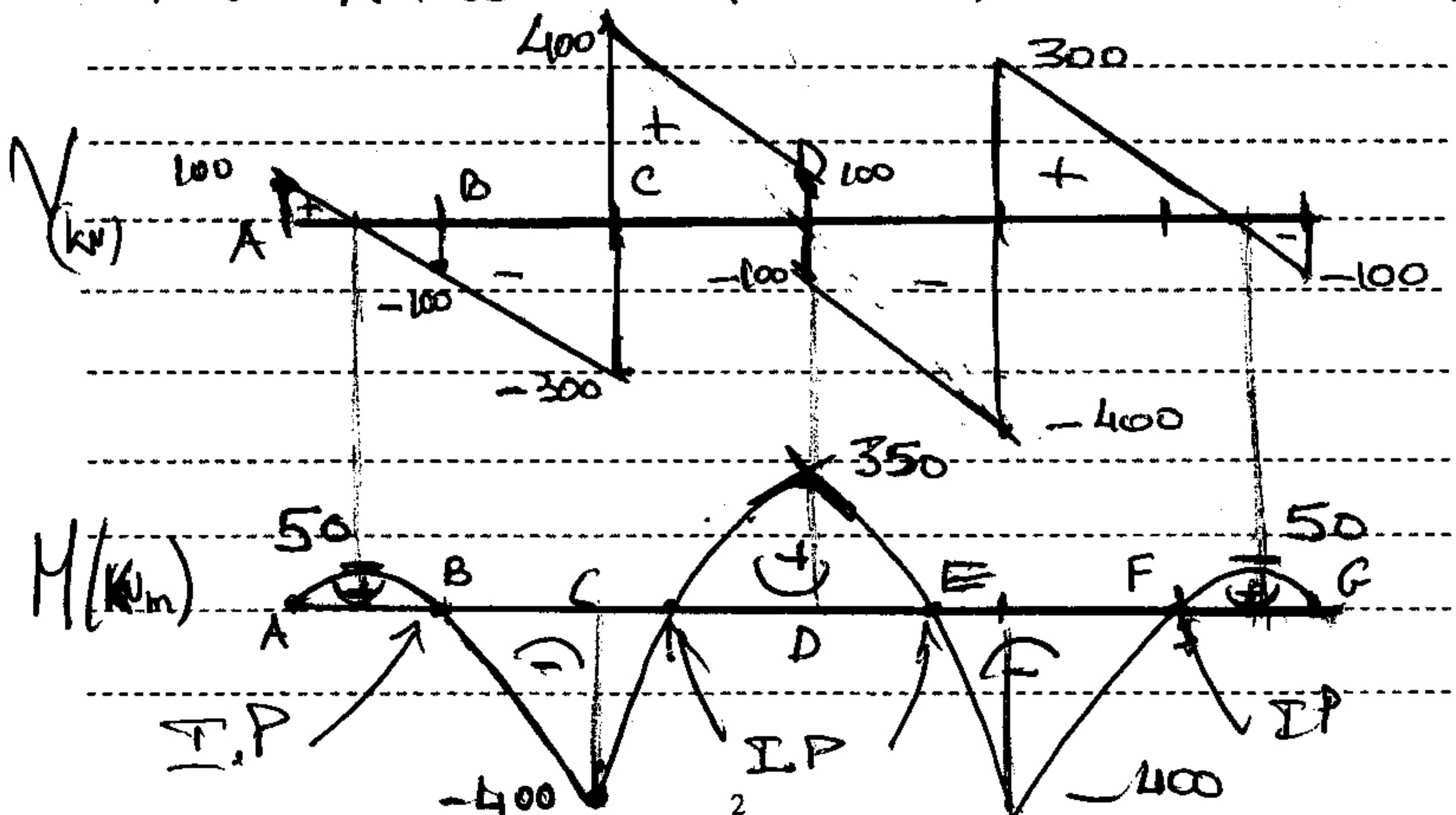
Referring to Figure I, let  $EI=200,000 \text{ kN.m}^2$  throughout the beam. Neglect the own weight of the beam.

**NOTE: THE SYSTEM IS SYMMETRICAL; YOU MAY TAKE ADVANTAGE OF THIS.**

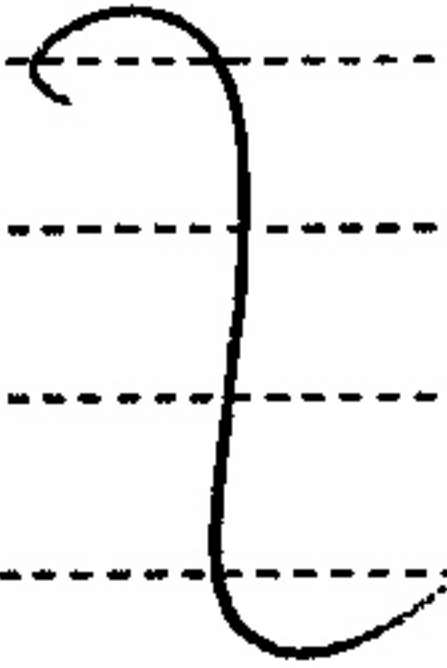
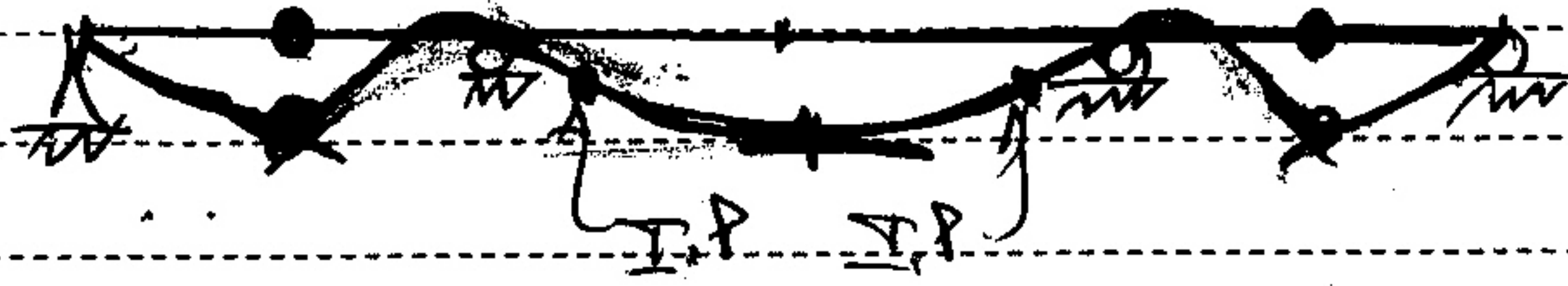
1. Calculate the reactions, and draw the shear and bending moment diagrams. (15 points)   
 Sketch a reasonable deflected shape showing important features (deflections, slopes, inflections, ...). (5 points)

Calculations and Diagrams:

$100 \text{ kN/m}$   
 $M=0$   
 $R_A \uparrow \quad 2m \quad B$   
 $\sum M_B = 0 \Rightarrow R_A \times 2 = 100 \times 2^2 / 2$   
 $\Rightarrow R_A = 100 \text{ kN} \uparrow \Rightarrow R_G = 100 \text{ kN} \uparrow$  (Symmetry)  
 Total load =  $200 + 100 \times 14 = 1600 \text{ kN}$   
 $\Rightarrow 2R_A + 2R_C = 1600 \text{ kN} \Rightarrow R_C = R_E = 700 \text{ kN} \uparrow$

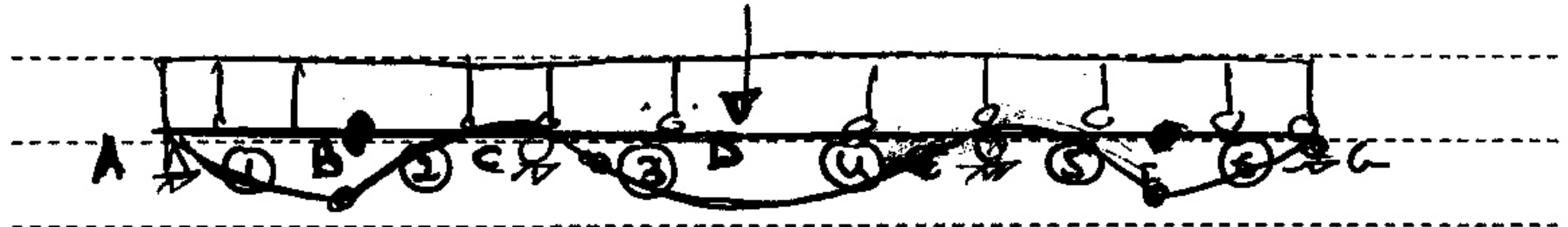


Calculations and/or Diagrams (cont'd):



2. Indicate how you would solve for the deflected shape using the method of INTEGRATION (Do not compute or write detailed equations; show an outline of the steps required). (10 points)

Calculations and Diagrams:



Curv.  $N'' = \frac{M}{EI}$

Slope  $N'(x) = \int N''(x) \rightarrow C_1$

Def  $N(x) = \int N'(x) \rightarrow C_2$

	A	B	C	D	E	F	G
	$M_1(x)$	$M_2(x)$	$M_3(x)$	$M_4(x)$	$M_5(x)$	$M_6(x)$	
	$N''_1(x)$	$N''_2(x)$					$N''_6(x)$
	$A_1$	$B_1$	$C_1$	$D_1$	$E_1$	$F_1$	
	$A_2$	$B_2$	$C_2$	$D_2$	$E_2$	$F_2$	

12 eqs  $\rightarrow$  12 Boundary Conditions  $\rightarrow$  12 Equations?

6 eqs

$N''_1(A) = 0$        $N''_3(C) = 0$        $N''_4(E) = 0$        $N''_6(G) = 0$   
 $N''_3(C) = 0$        $N''_5(E) = 0$

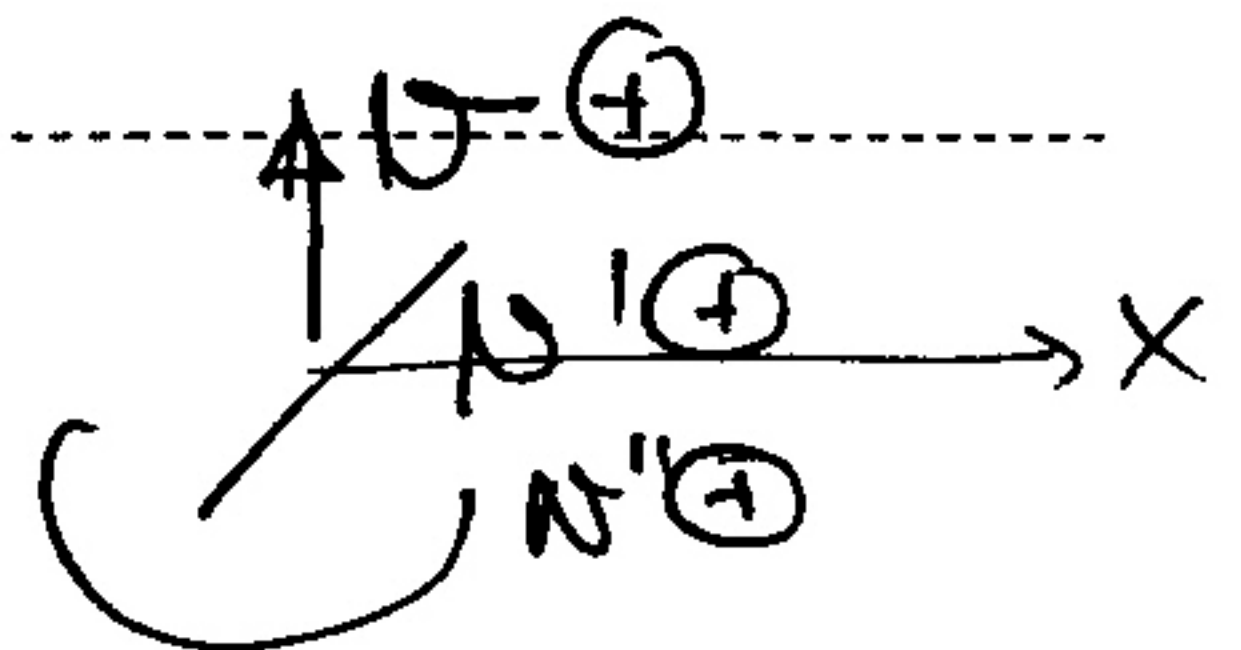
3 eqs

$N'_2(C) = N'_3(C)$        $N'_4(E) = N'_5(E)$   
 $N'_3(D) = N'_4(D)$

3 eqs

$N_2(B) = N_3(B)$        $N_3(D) = N_4(D)$        $N_5(F) = N_6(F)$

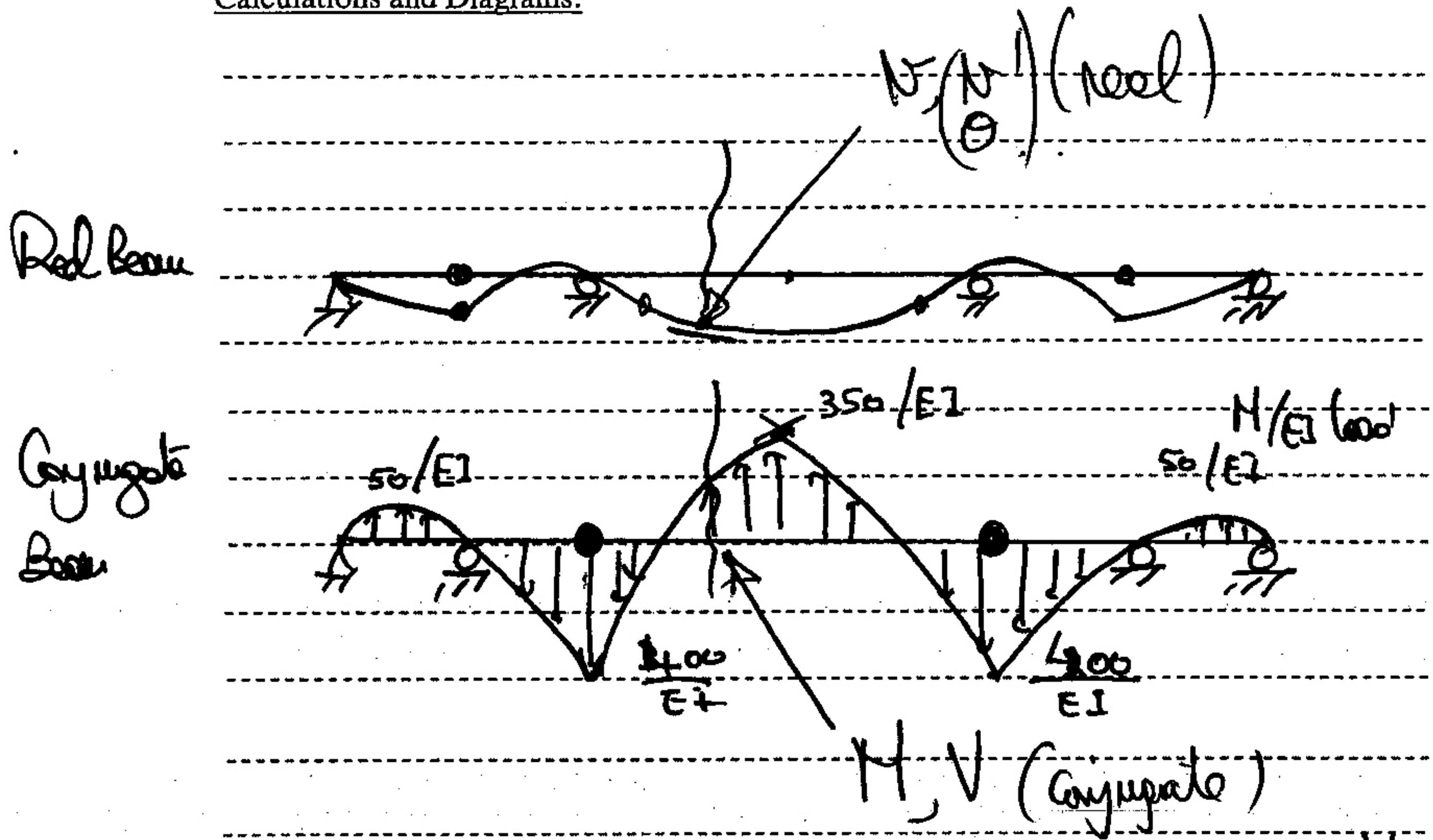
Solve for  $A_1, \dots, F_2$





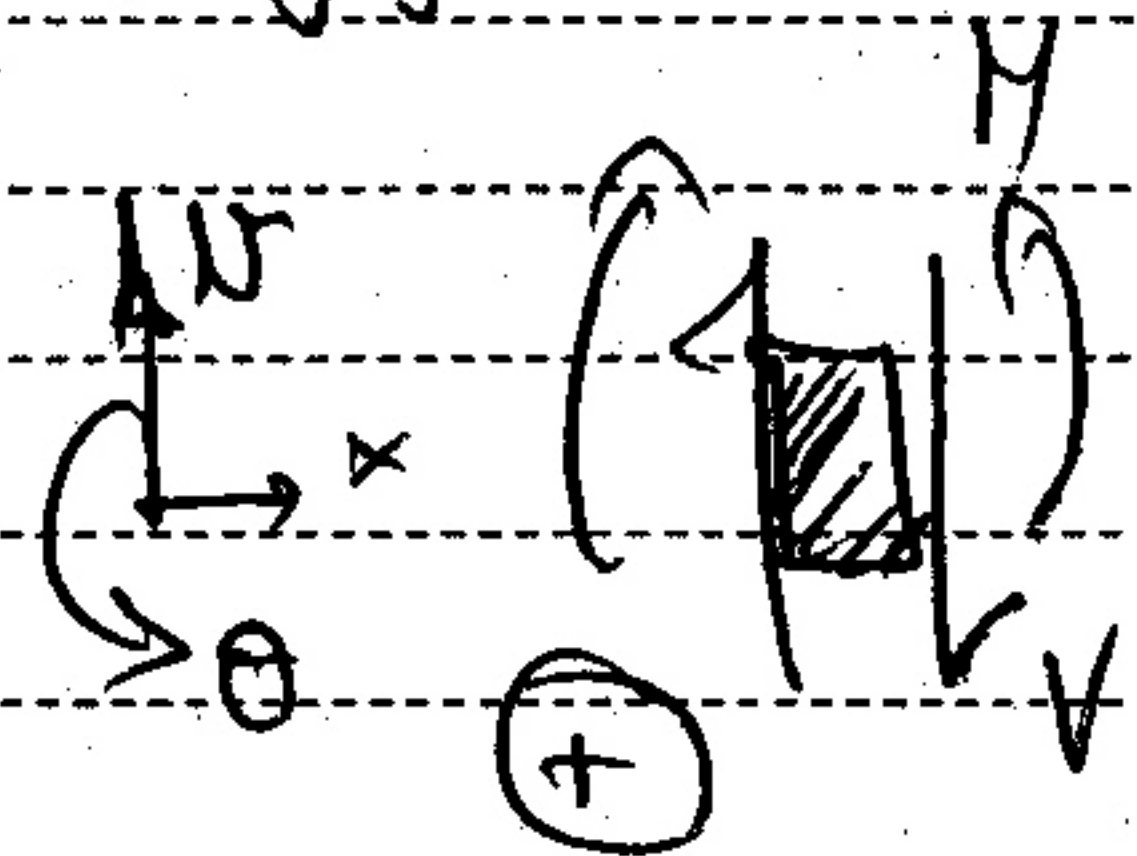
3. Draw the CONJUGATE BEAM with the corresponding load. Explain in two lines how you would solve for a deflection and slope at a point (Do not solve). (5 points)

Calculations and Diagrams:



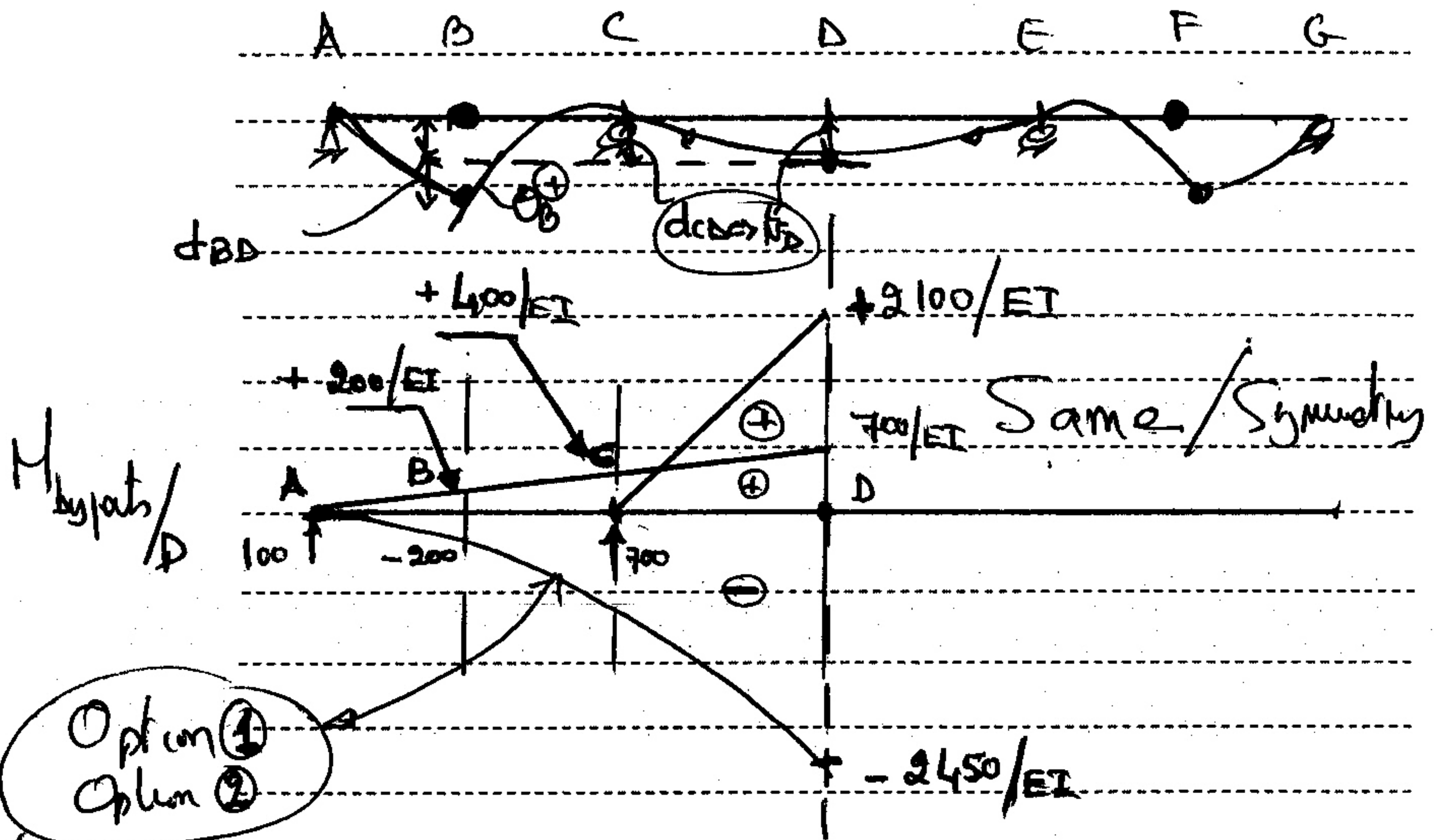
$$N_{real} = M_{conjugate}$$

$$\theta_{real} = N'_{real} = V_{conjugate}$$



4. Using the MOMENT-AREA METHOD, compute the vertical deflections and slopes at points B and D (Again, symmetry can help here). Is the vertical deflection at B maximum between A and C; why or why not? (30 points)

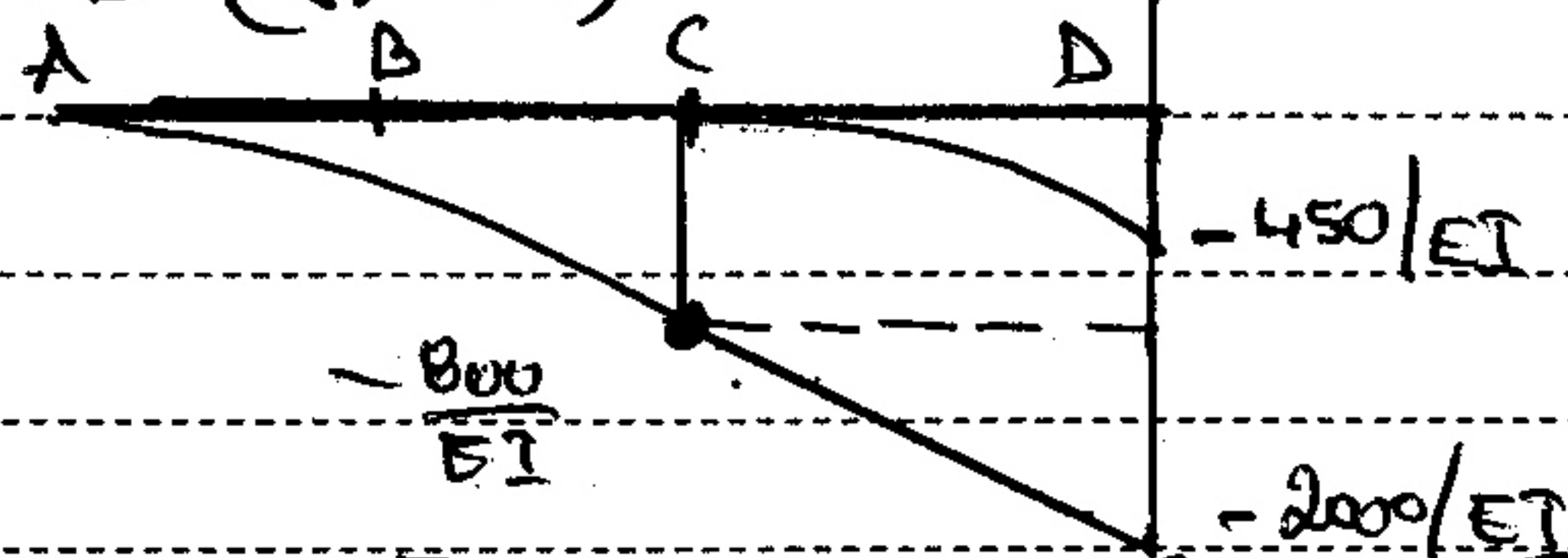
Calculations and Diagrams:



$\theta_B, \theta_D, \theta_B^-, \theta_B^+, \theta_D$

$\theta_D = 0$  (Symmetry)

$d_{CD} \Leftrightarrow \theta_B$



Point  $\rightarrow$

$$d_{CD} = \frac{1}{EI} \left[ \left( \frac{1}{2} \right) (2100) (3) \left( \frac{2}{3} \times 3 \right) + \left( \frac{1}{2} \right) (300) (3) \left( \frac{2}{3} \times 3 \right) + (1) (400) (3) \left( \frac{1}{2} \times 3 \right) \right. \\ \left. + \left( \frac{1}{2} \right) (-800) (3) \left( \frac{2}{3} \times 3 \right) + (1) (-800) (3) \left( \frac{1}{2} \times 3 \right) + \left( \frac{1}{3} \right) (-450) (3) \left( \frac{3}{4} \times 3 \right) \right]$$

$$= + \frac{787.5}{EI}$$

(6)

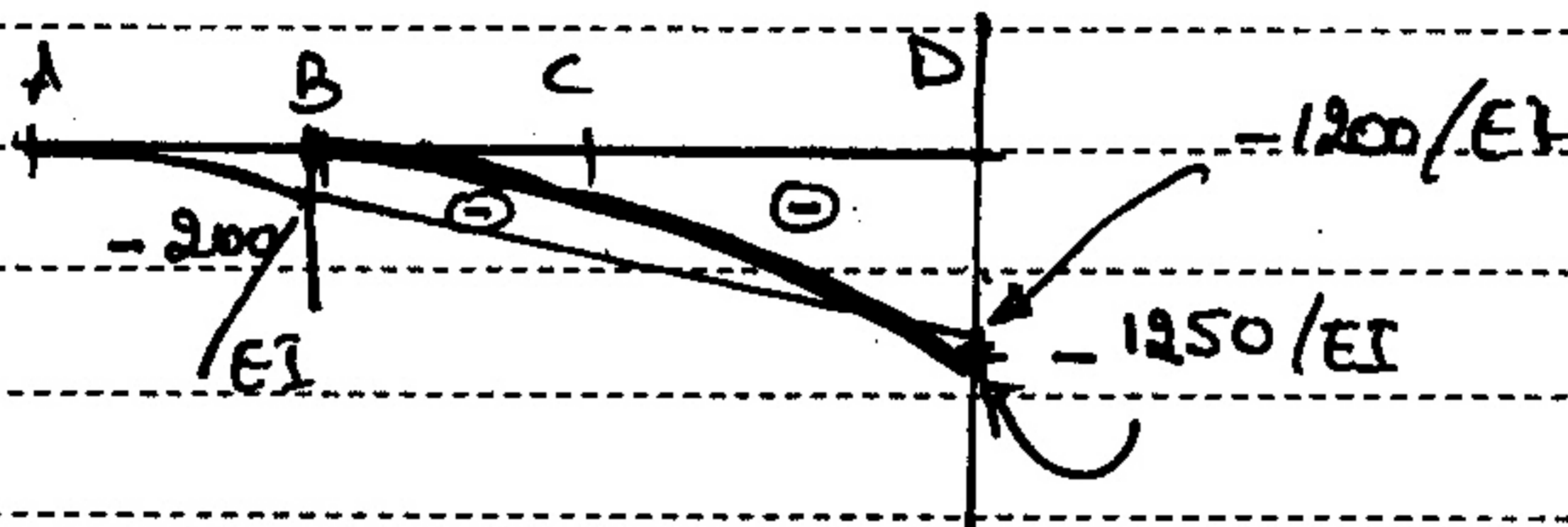
Calculations and/or Diagrams (cont'd):

$$d_{CD} = \frac{\oplus 787.5}{EI} = 3.94 \times 10^{-3} \text{ m} \quad \oplus \text{ Point C Above } \checkmark$$

$$\boxed{N_D = 3.94 \times 10^{-3} \text{ m} \downarrow}$$

$$\ominus \ominus \ominus : \quad \ominus \ominus \ominus - \ominus \ominus \ominus = \text{Area } M_{D \rightarrow B}$$

Option 2

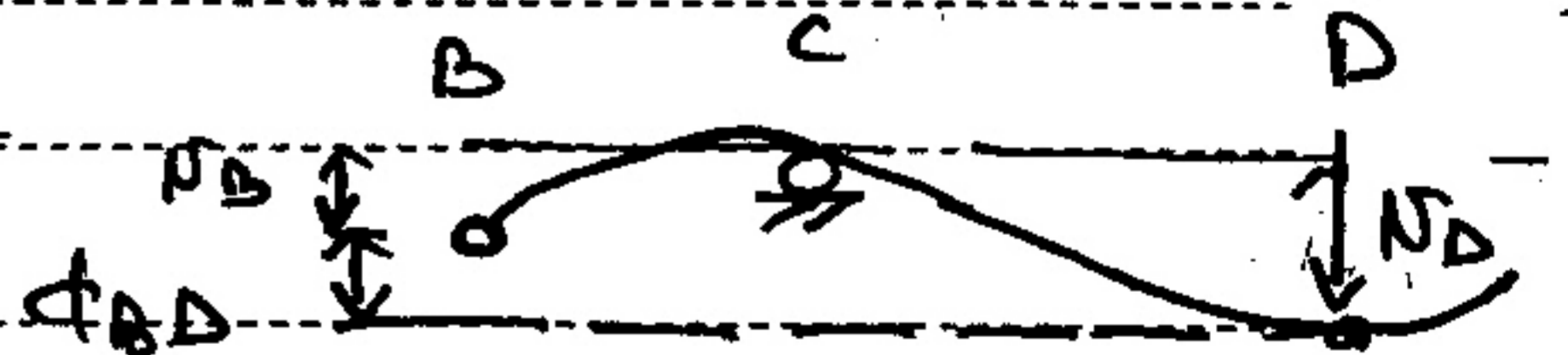


$$\begin{aligned} \ominus \ominus \ominus - \ominus \ominus \ominus &= \frac{1}{EI} \left[ \left( \frac{1}{2} \right) (-1200 - 200) (5) + \left( \frac{1}{3} \right) (-1250) (5) \right. \\ &\quad \left. + \left( \frac{1}{2} \right) (200) (3) + \left( \frac{1}{2} \right) (700 + 200) (5) \right] = -\frac{183.32}{EI} \end{aligned}$$

$$\boxed{\ominus \ominus \ominus \ominus = +0.917 \times 10^{-3} \text{ rad} \Rightarrow \text{C.C.W.} \checkmark}$$

$$\begin{aligned} d_{BD} &= \frac{1}{EI} \left[ \left( \frac{1}{2} \right) (-1200 + 200) (5) \left( \frac{2}{3} \times 5 \right) + \left( \frac{1}{3} \right) (-200) (5) \left( \frac{1}{2} \times 5 \right) + \left( \frac{1}{3} \right) (-1250) (5) \left( \frac{2}{3} \times 5 \right) \right. \\ &\quad \left. + \left( \frac{1}{2} \right) (200) (3) \left( 2 + \frac{2}{3} \times 3 \right) + \left( \frac{1}{2} \right) (700 - 200) (5) \left( \frac{2}{3} \times 5 \right) + \left( \frac{1}{2} \right) (200) (5) \left( \frac{1}{2} \times 5 \right) \right] \end{aligned}$$

$$= \frac{\oplus 620.8}{EI} \text{ Point B Above}$$



$$|N_B| = |N_D| = |d_{BD}| = \frac{787.5}{EI} - \frac{620.8}{EI} = \frac{166.7}{EI} \downarrow$$

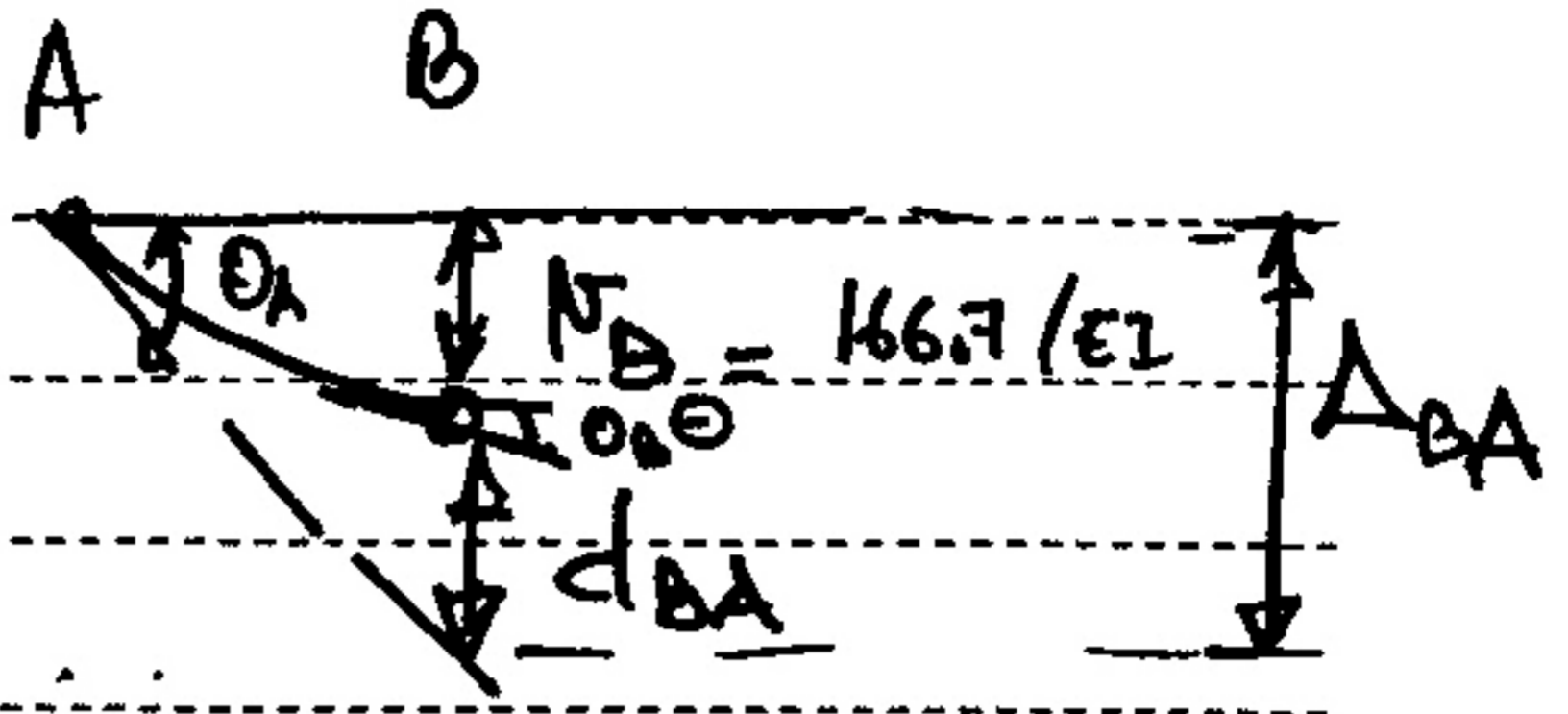
$$\boxed{N_B = 0.833 \times 10^{-3} \text{ m} \downarrow}$$



Calculations and/or Diagrams (cont'd):

Point  $\Delta_{BA} = \frac{1}{EI} \left[ \left( \frac{1}{2} \right) (200) (2) \left( \frac{1}{3} \times 2 \right) + \left( \frac{1}{3} \right) (200) (2) \left( \frac{1}{4} \times 2 \right) \right]$

$= \frac{+66.67}{EI}$   $\oplus$  Point Above  $\checkmark$



$\Delta_{BA} = \frac{233.3}{EI} \Rightarrow |\Theta_A| = \frac{|\Delta_{BA}|}{2} = \frac{116.67}{EI}$  C.W.  $\ominus$

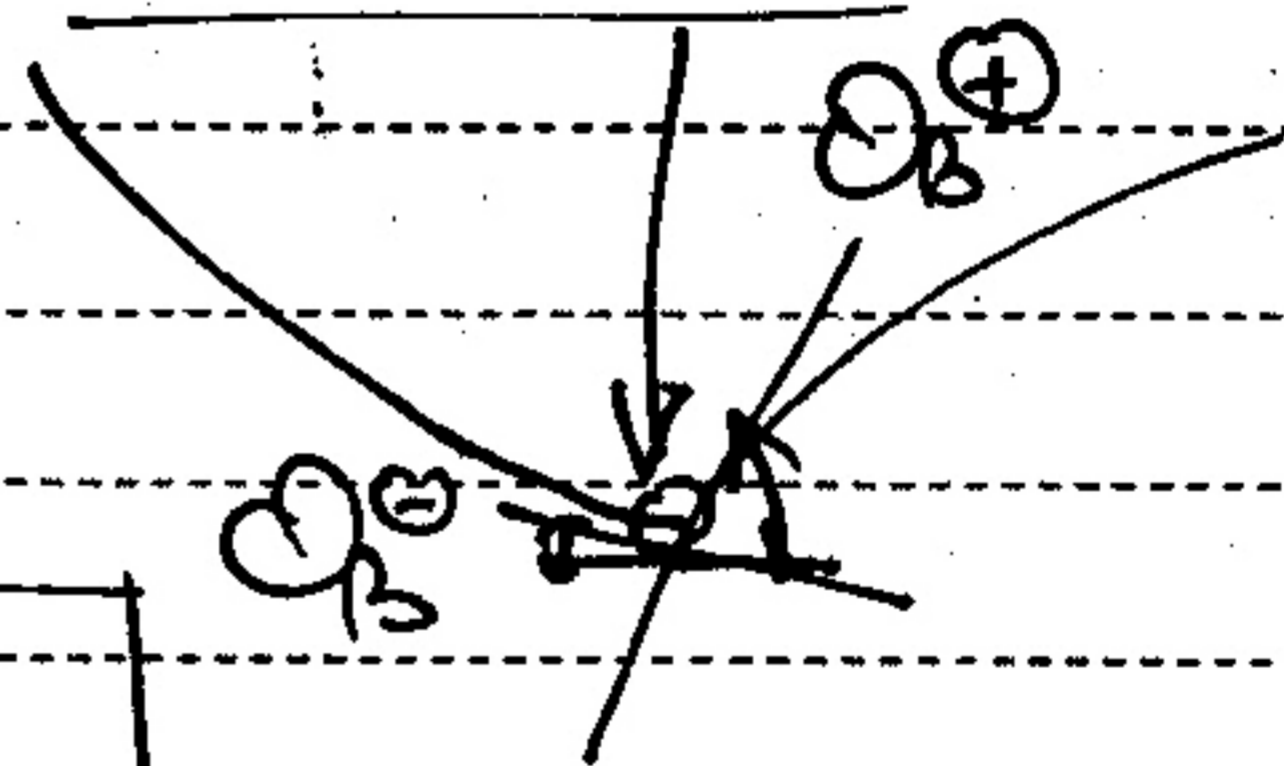
$\Theta_B^{\ominus} - \Theta_A = \frac{1}{EI} \left[ \left( \frac{1}{2} \right) (200) (2) + \left( \frac{1}{3} \right) (-200) (2) \right] = + \frac{66.67}{EI}$

$\Rightarrow \Theta_B^{\ominus} = \frac{1}{EI} (66.67 + \Theta_A) = \frac{(66.67 - 116.67)}{EI} = - \frac{50}{EI}$  CW

$\Theta_B^{\ominus} = -0.00025 \text{ rad} = -0.25 \times 10^{-3} \text{ rad CW}$

$\Theta_B^{\ominus} \rightarrow \ominus \text{ CW}$

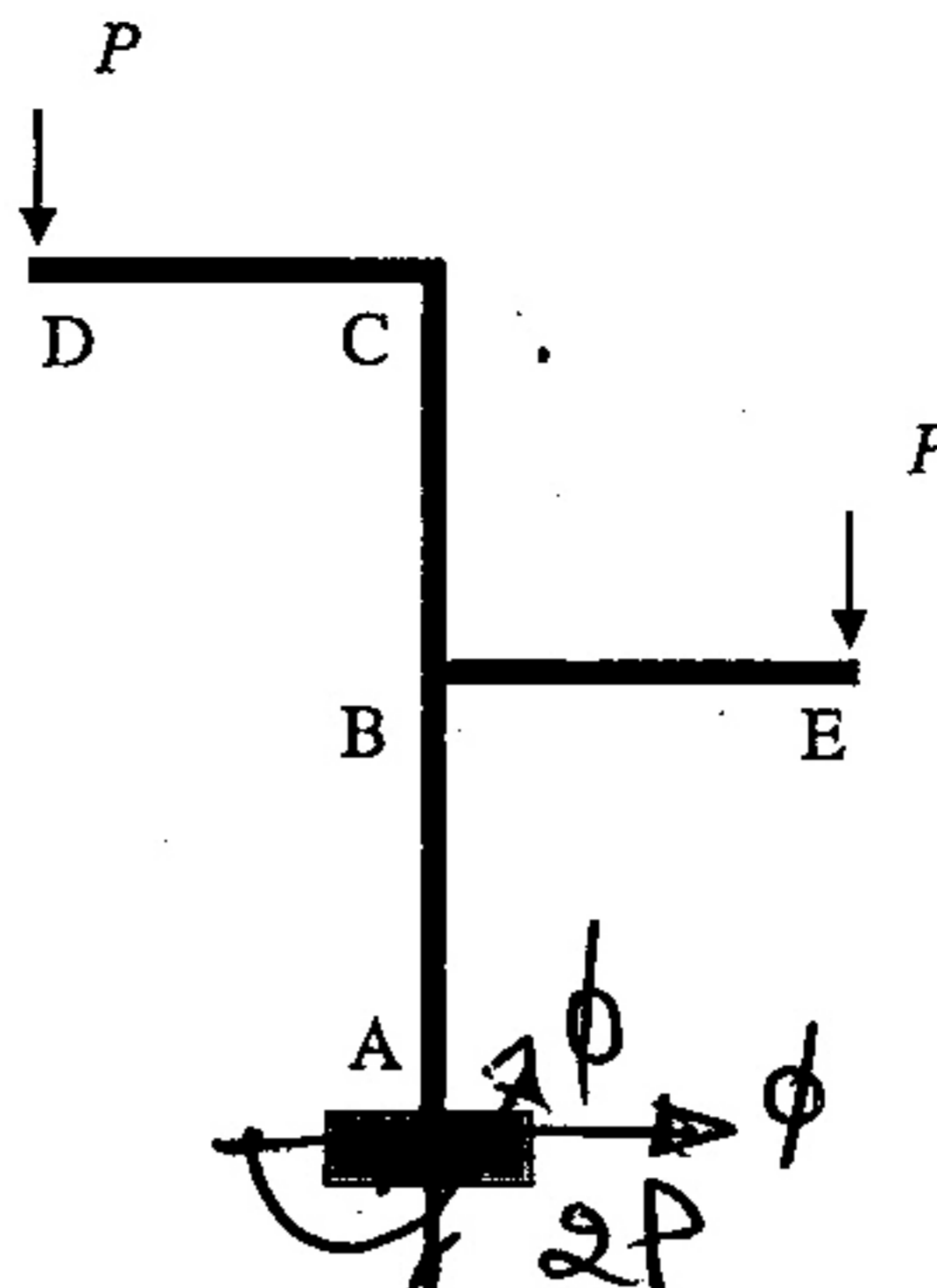
$\Theta_B^{\oplus} \rightarrow \oplus \text{ CCW}$



$\Rightarrow N_B \text{ max between A} \rightarrow \text{C}$



**Problem II: (35 points)**



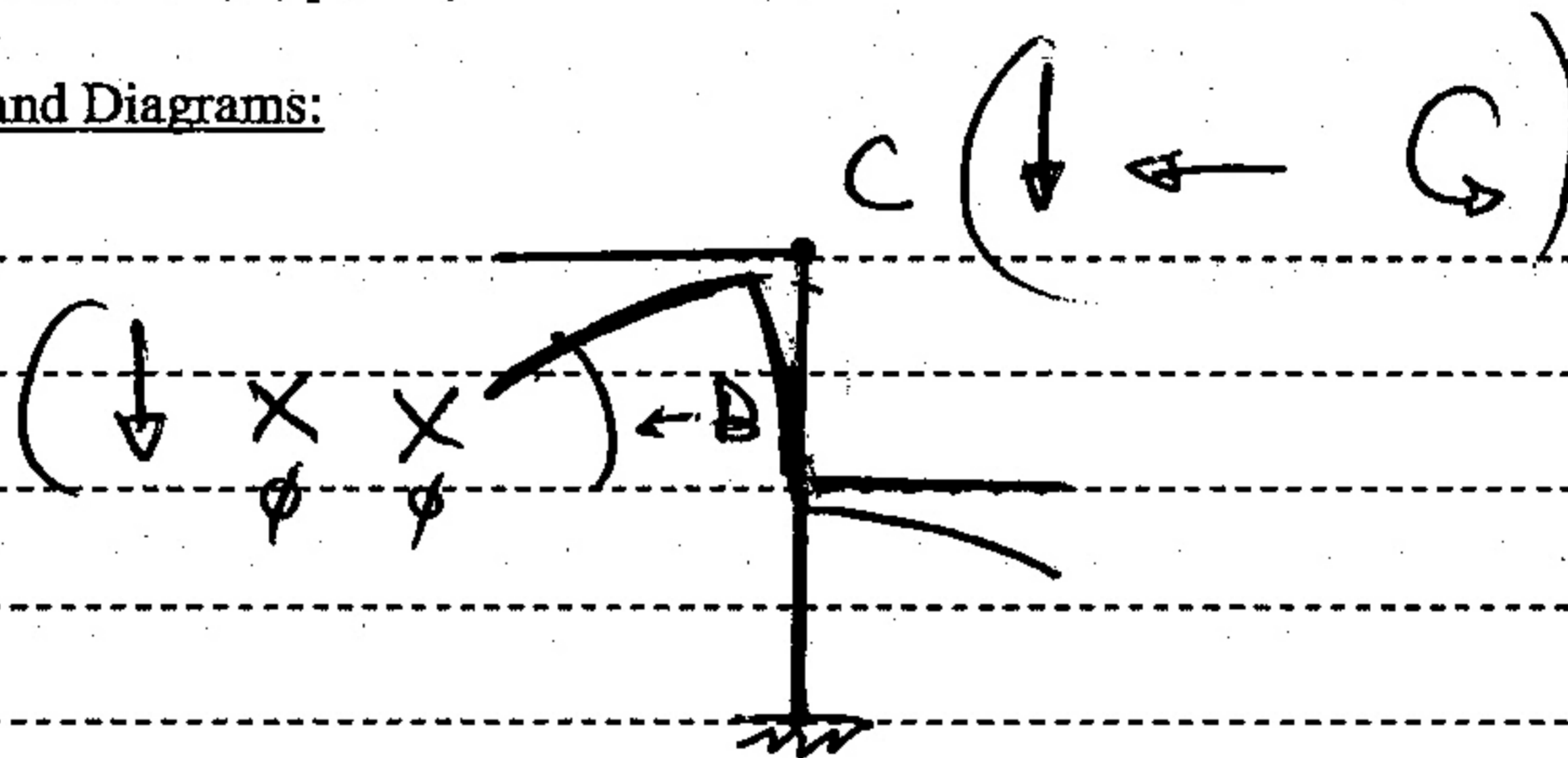
Reactions

Figure II

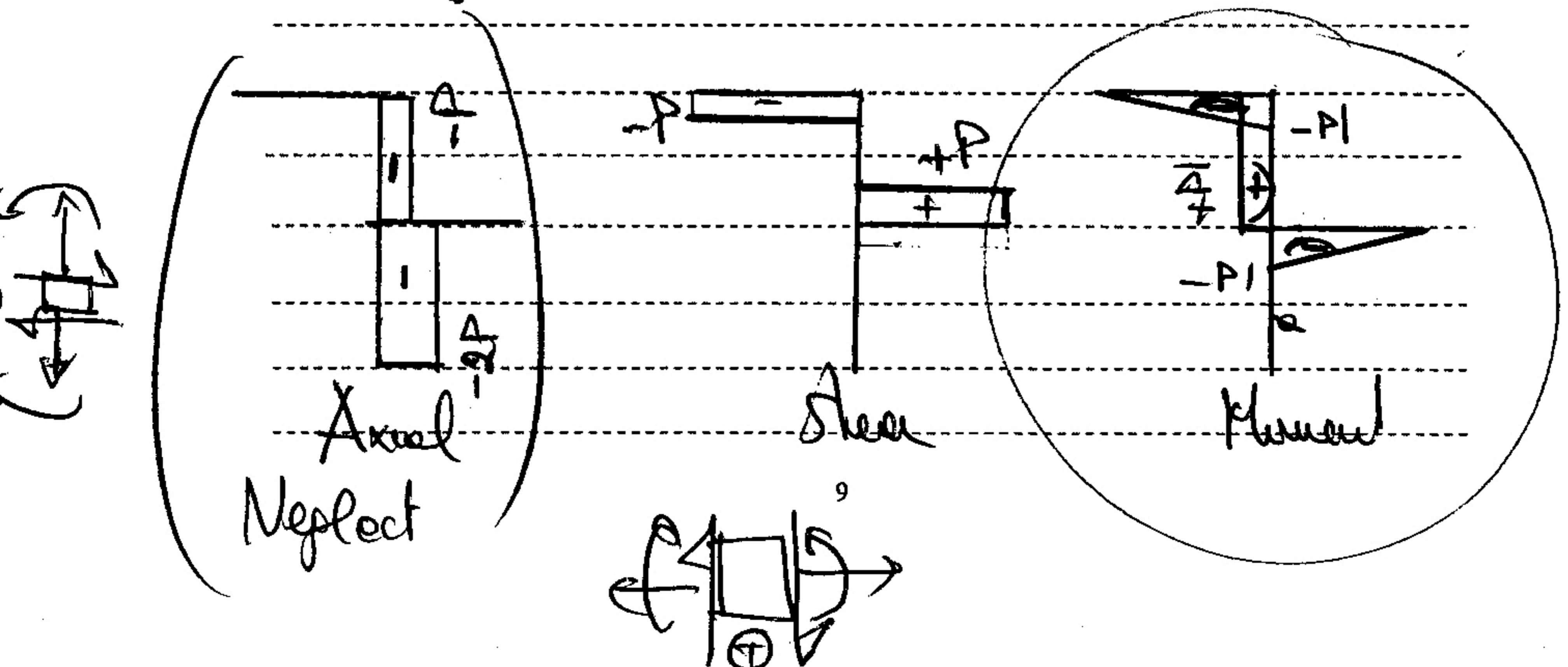
Referring to Figure II, the frame members have AB, BC, CD, and BE have the same length  $L$ . Neglect the own weight of the frame.

- Let all members have the same  $EI$ . Predict, without calculations, the direction of deflections/rotations of joints B and C (up or down, left or right, cw or ccw), and sketch your predicted deflected shape of the frame. (5 points)
- Neglecting axial deformations, compute the deflections/rotations in all joints, and compare with your predictions. (15 points)

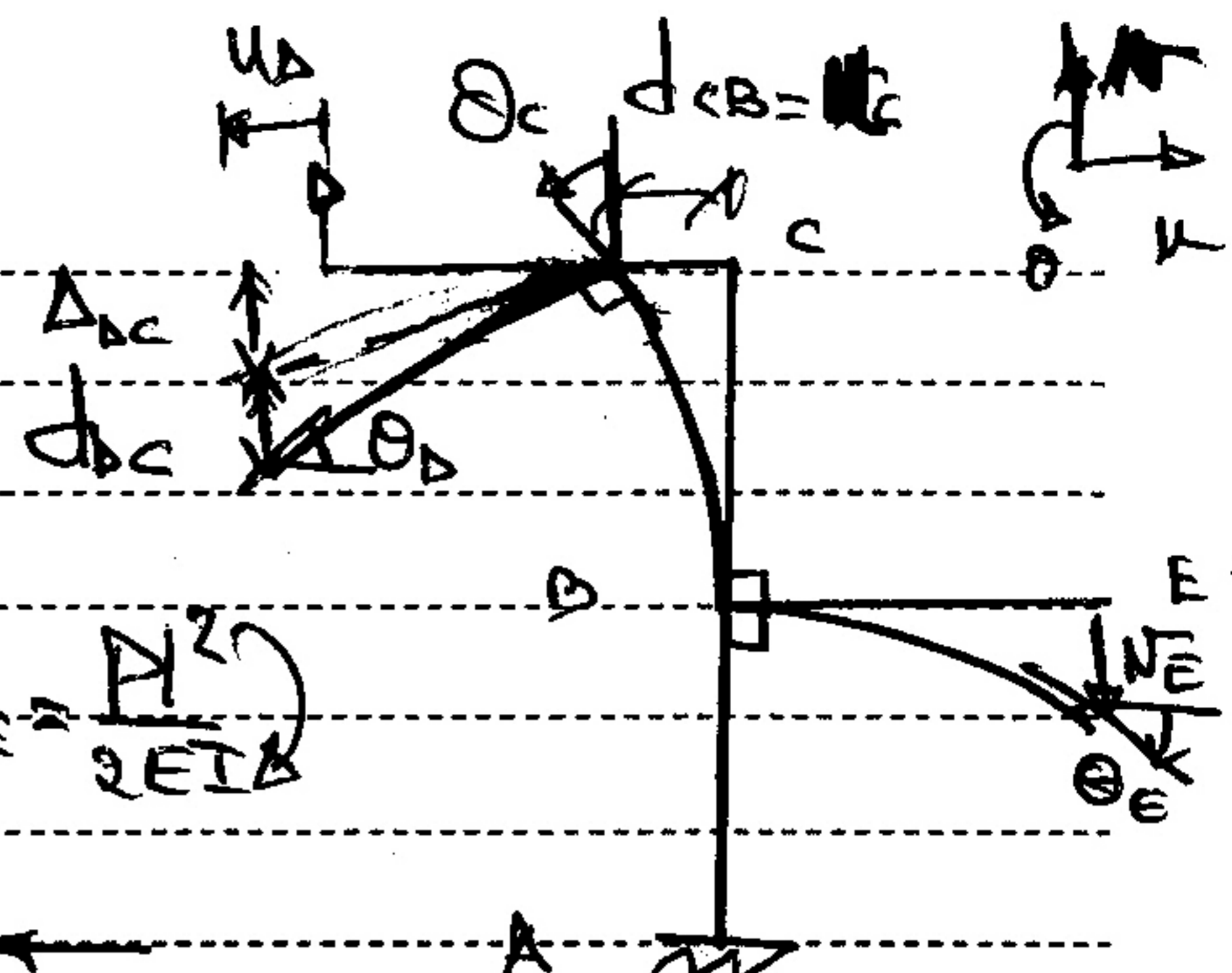
Calculations and Diagrams:



Neglecting Axial Deformation



Calculations and/or Diagrams (cont'd):



$M_A = N_A = \theta_A = 0$  (fixed)

$u_B = v_B = \theta_B = 0$

$u_E = 0$   $N_E = \frac{Pl^3}{3EI}$   $\theta_E = \frac{Pl^2}{2EI}$

$N_C = 0$   $N_{CD} = |d_{CD}| = \frac{Pl^3}{2EI}$

$\theta_C = \frac{Pl^2}{EI}$  (Axial Def  $\rightarrow 0$ )

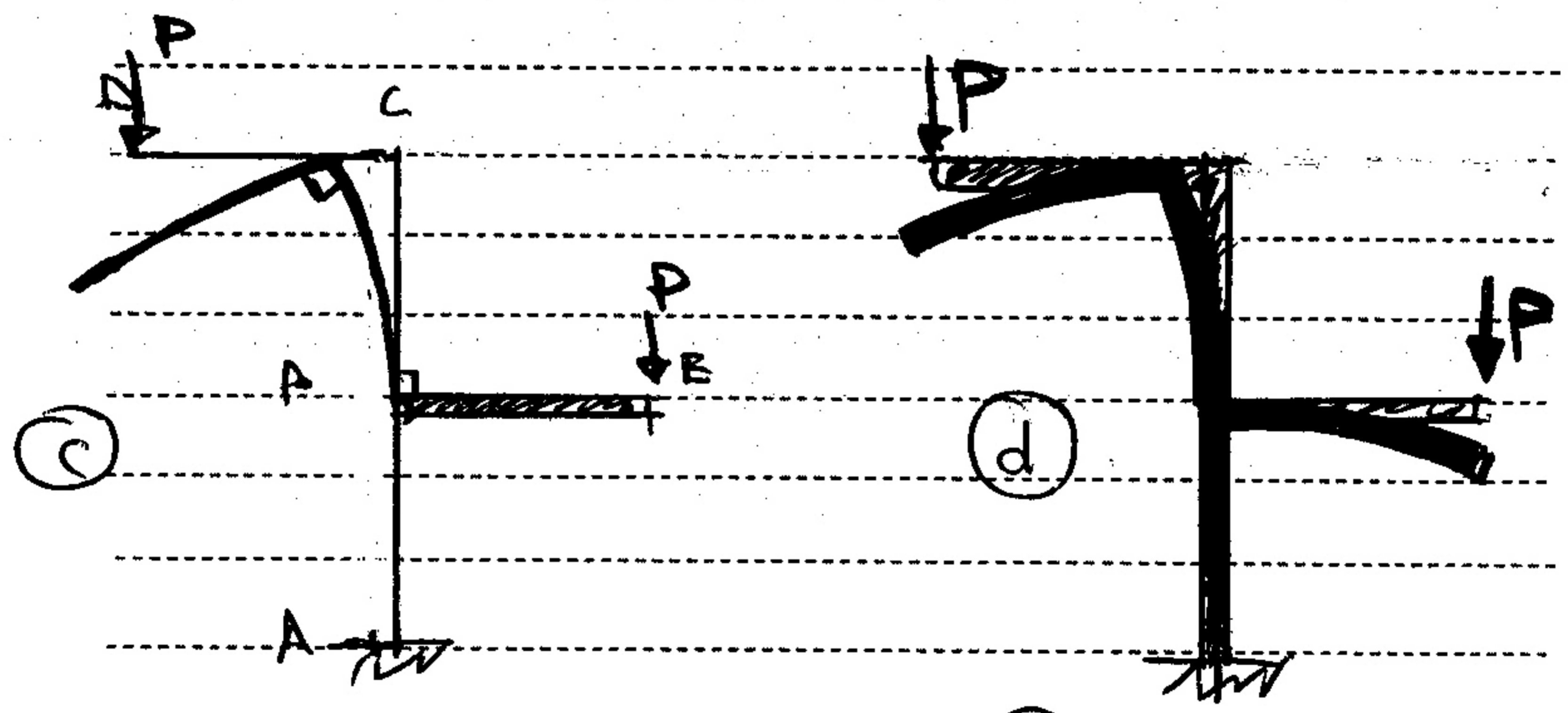
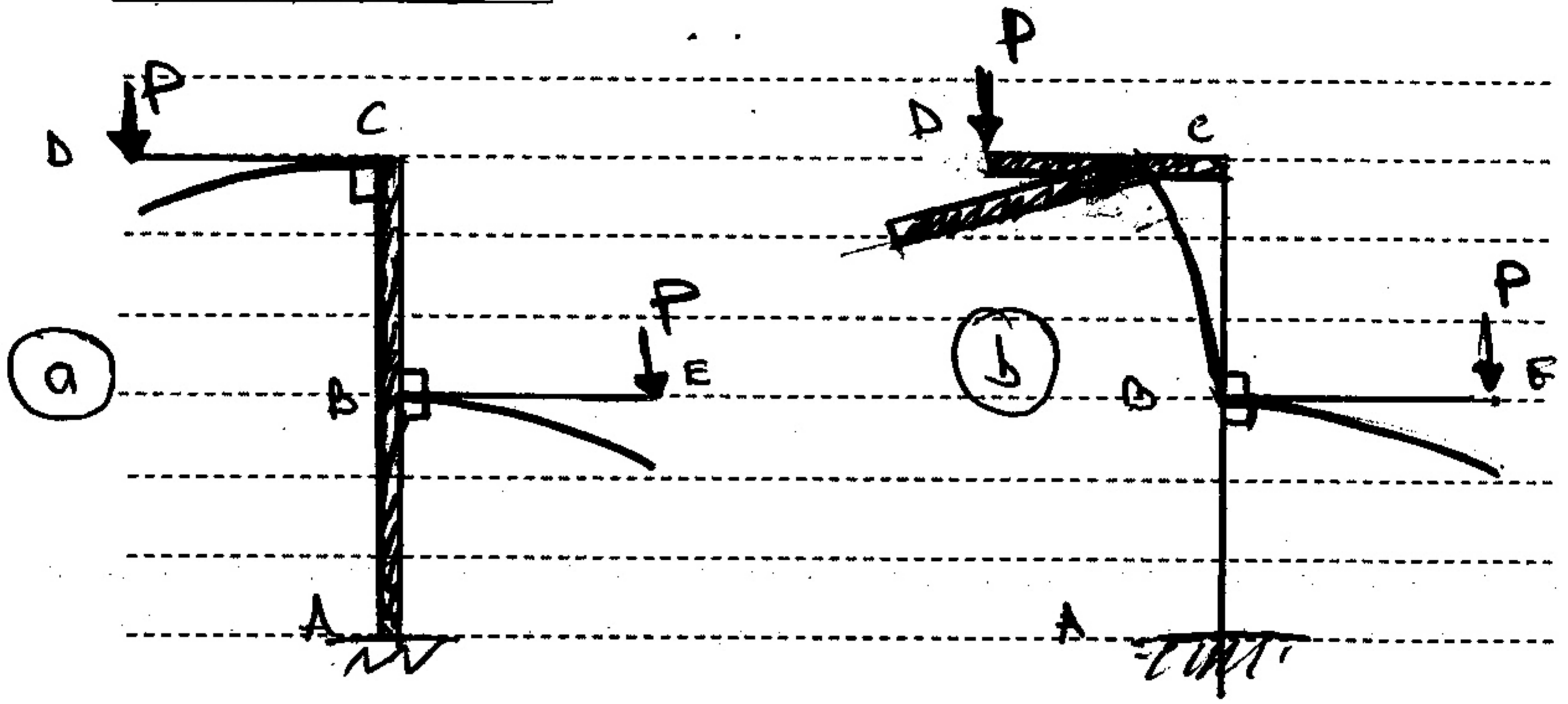
$M_D = N_C = \frac{Pl^3}{2EI}$

$|N_D| = |N_{DC} + d_{DC}| = \theta_C \times l + \frac{Pl^3}{3EI} = \frac{4Pl^3}{3EI}$

2. Sketch the deflected shapes for the frames under the following conditions: (15 points)
  - a. Member ABC is very stiff (all other members are normal).
  - b. Member CD is very stiff (all other members are normal).
  - c. Member BE is very stiff (all other members are normal).
  - d. All members are very stiff.

✓  
✓  
✓  
✓

Calculations and Diagrams:



Same as question 1  
(with smaller values  
of deflections)

2