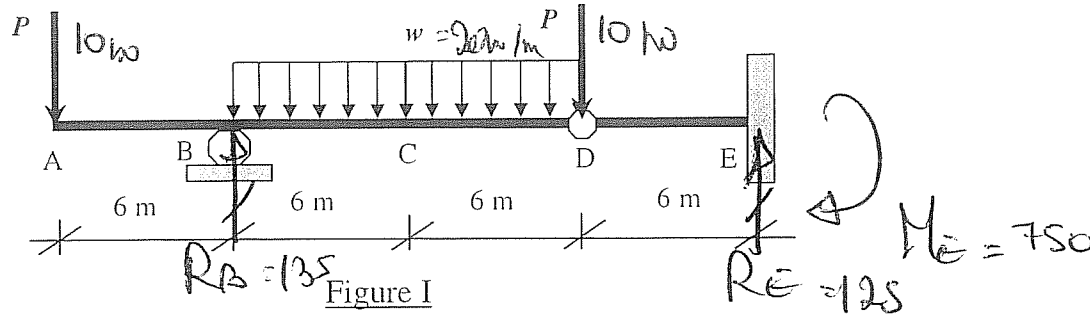


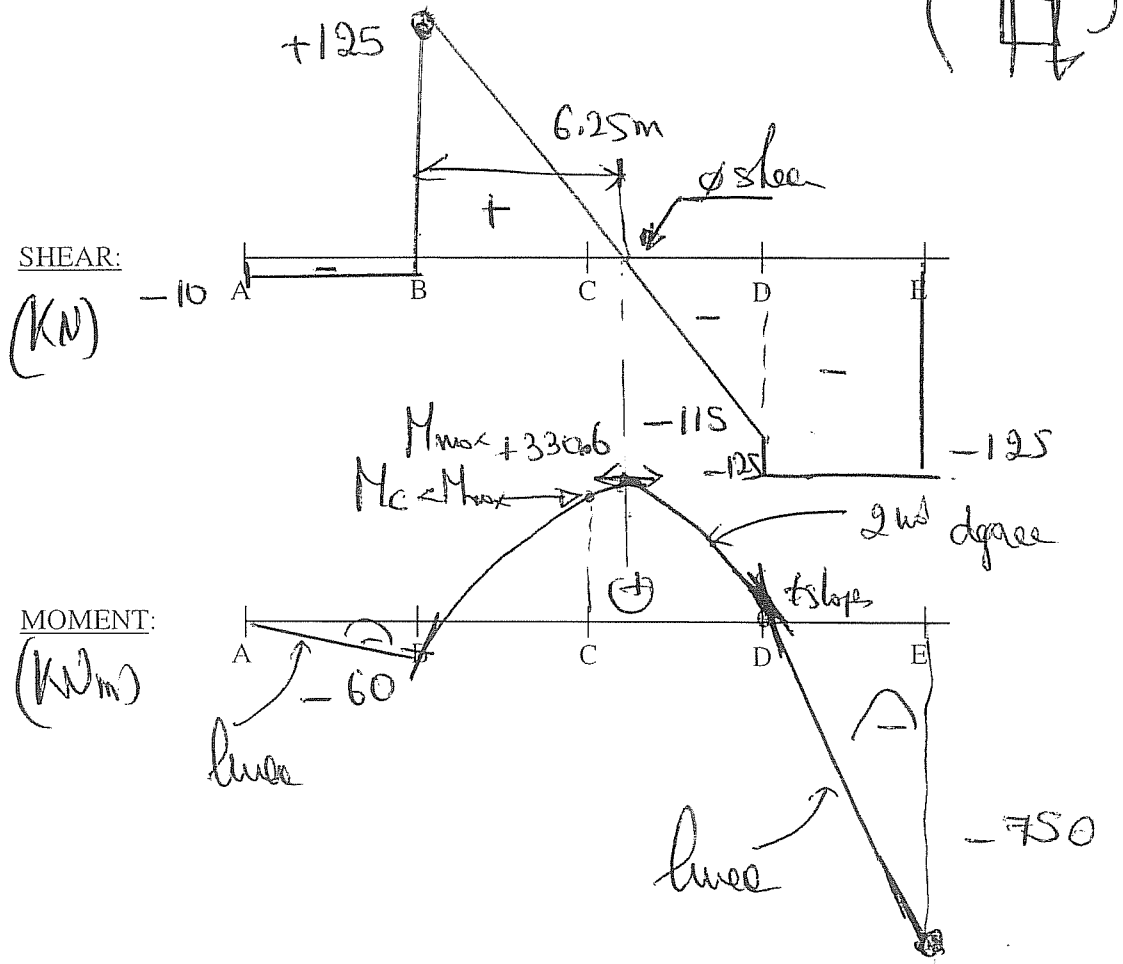


**Problem I/I:**



Referring to Figure I:  
 $EI=2,000,000 \text{ kN.m}^2$  throughout the beam (except in Question 4).  
 $w=20 \text{ kN/m}$  and  $P=10 \text{ kN}$  throughout the problem (except in Question 4).  
 Neglect the own weight of the beam.

1. Compute the reactions (forces and moments) in the beam, and draw the shear and bending moment diagrams. (15 points)



Calculations and/or Diagrams:

$$\text{Considering AD: } \sum M_B = 0$$

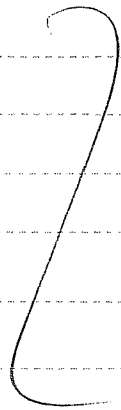
$$\Rightarrow R_B \times 12 = 10 \times 18 + \frac{20 \times 12^2}{2}$$

$$\Rightarrow R_B = 135 \text{ kN } \uparrow$$

$$\text{Considering AE } \sum F_y = 0$$

$$\Rightarrow R_E = 10 + 10 + 20 \times 12 - 135 = 195 \text{ kN } \uparrow$$

$$\sum M_E = 0 \Rightarrow M_E = 10 \times 24 + 20 \times 12 \times 12 + 10 \times 6 - R_B \times 18 = 750 \text{ kN } (\rightarrow)$$



2. USING THE MOMENT-AREA METHOD

Based on the moment diagram in question 1, sketch a reasonable deflected shape. (2 points)

In what follows, you can calculate slope and deflections in the order you find suitable.

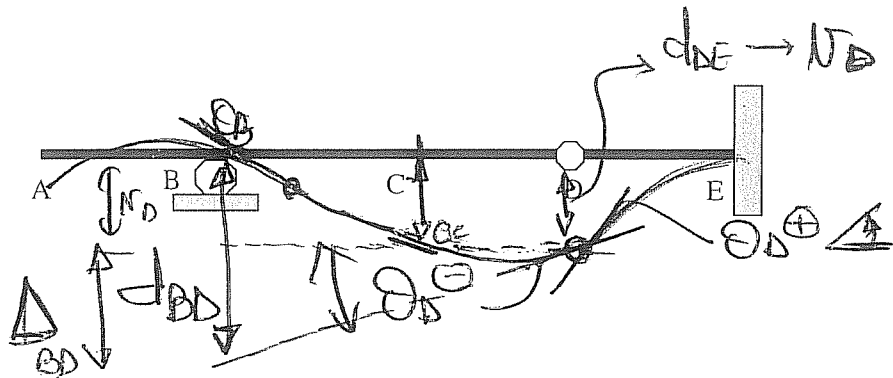
Compute the slopes  $\theta$  and vertical deflections  $v$  at all points A, B, C, D, and E. (35 points)

Compute the maximum downward deflections:

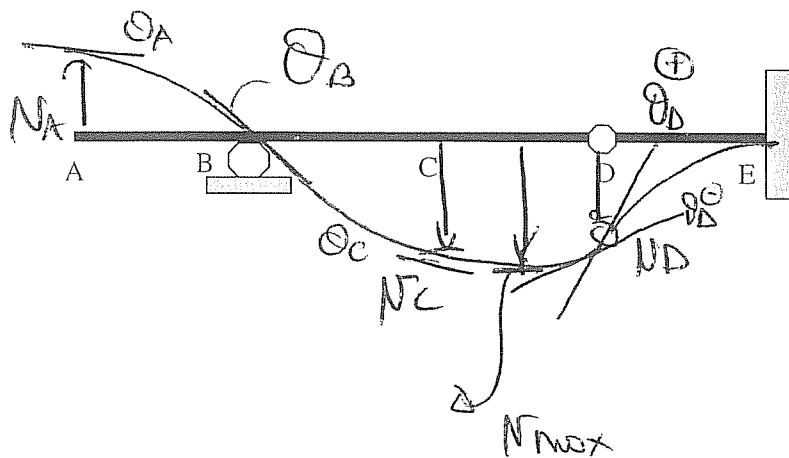
- (i) between D and E. (5 points)
- (ii) between B and D. (10 points)  → Explain how you estimate

Based on the results obtained, neatly/clearly sketch the final deflected shape and show the results obtained. (3 points)

INITIAL DEFLECTION



FINAL DEFLECTION



Calculations and/or Diagrams:

Considering DE  $N_E + \theta_E = 0$  (fixed end)

$\frac{EI}{EI} (\theta_E - 0) = \frac{750}{EI} \Rightarrow \theta_D = + \frac{1}{2} (750)(6) \times \frac{1}{EI}$

$\theta_D = +0.001125 \text{ rad}$   
 C.C.W

$d_{DE} = \frac{2}{3} \times 6 = 4$

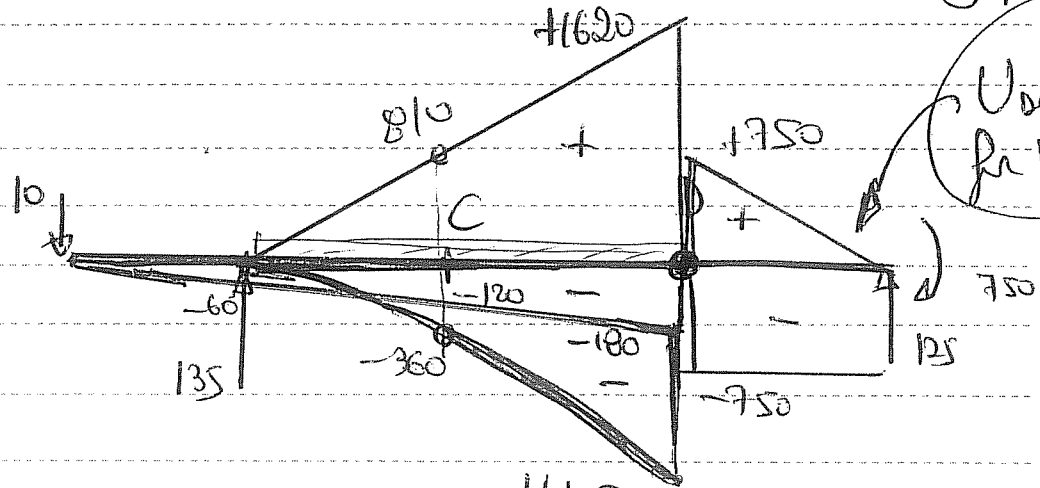
$d_{DE} = -0.001125 \times \left(\frac{2}{3} \times 6\right) = -0.0045 \text{ m}$   
 below top

$N_D = 0.0045 \text{ m}$   
 (4.5mm)

Considering AD

$d_{AD} (?) = \text{Mom by parts} \Rightarrow$

M  
 Wu  
 Feet/



check @ D:  $M^{\ominus} - M^{\oplus} = 0$

$EI d_{AD} = \frac{1}{2} (1620) \times (6) \left(\frac{2}{3} \times 6\right) - (60)(12) \times \left(\frac{1}{2} \times 12\right) - \frac{1}{2} (120)(12) \left(\frac{2}{3} \times 12\right) - \frac{1}{3} (1440)(12) \left(\frac{3}{4} \times 12\right)$

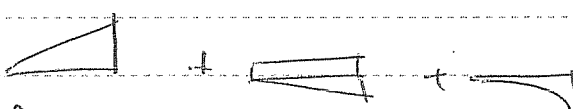
$\frac{9720}{5760} = \frac{15840}{EI} = +0.00792 \text{ m}$   
 (round Above)

Calculations and/or Diagrams (cont'd):

$$|\Delta_{DD}| - |d_{DD}| - |N_D| = 0.00792 - 0.0045 = 0.00342 \text{ m}$$

$$|\Theta_D| = \frac{0.00342}{12} = 0.000285 \text{ rad}$$

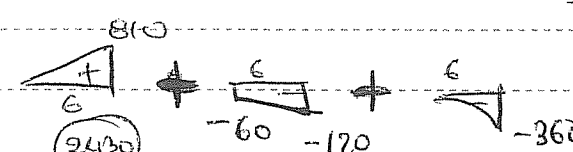
$$\Theta_D = -0.000285 \text{ rad (CW)}$$

Eq  $(\Theta_D - \Theta_B) =$  

$$\Rightarrow EI \Theta_B = EI \Theta_D - 2520 \Rightarrow \Theta_B = \frac{570 - 2520}{EI} = -\frac{1950}{EI}$$

Roller  $N_B = 0$

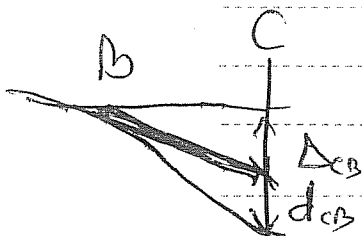
$$\Theta_B = -0.000775 \text{ rad (CW)}$$

$$EI (\Theta_C - \Theta_D) =$$


$$= \left(\frac{1}{2}\right)(810)(6) - \frac{1}{2}(60+120)(6) - \frac{1}{3}(360)(6)$$

$$\Rightarrow EI \Theta_C = EI \Theta_D + 195 = -1950 + 1170 = -780$$

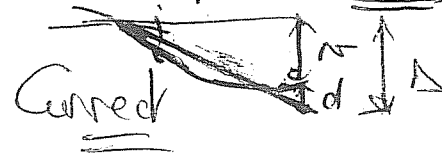
$$\Rightarrow \Theta_C = -0.00039 \text{ rad (CW)}$$



$$d_{CB} = \Delta_{CB} = |\Theta_B| \times 6 = 0.00585$$

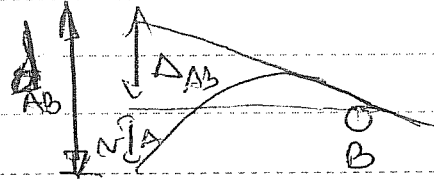
$$N_C = \Delta - |d|$$

$$N_C = 0.00468 \text{ m}$$



Calculations and/or Diagrams (cont'd):

$N_A$   
 $\theta_A$



$$EI(\theta_B - \theta_A) = \int_0^L M dx = \int_0^6 (-60) dx = \left(\frac{1}{2}\right)(-60)(6) = -180$$

$$\rightarrow \theta_A = \theta_B + \frac{180}{EI} = \frac{-1450 + 180}{EI} = \frac{-1270}{EI} = \theta_A \text{ below B}$$

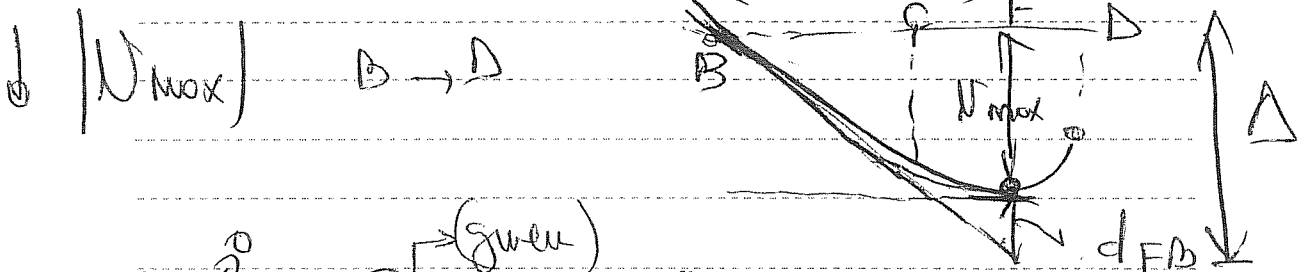
$$EI d_{AB} = \int_0^L \int_0^x M dx dx = \int_0^6 \left(\frac{1}{2}\right)(-60)(x)(\frac{2}{3}x) dx = -720$$

$\Rightarrow d_{AB} = -\frac{720}{EI}$

$$\Delta_{AB} = |\theta_B| \times 6 = \frac{11,700}{EI} = \frac{10980}{EI}$$

$$N_A = |A| - [d] = \frac{11700 - 720}{EI} = \boxed{0.00549 \text{ m} = N_A \uparrow}$$

$\downarrow N_{max}$  D  $\rightarrow$  E =  $N_D = 0.0025$



$$\theta_{F_{max}} - \theta_B = \int_0^{X_{max}} M dx = \int_0^{X_{max}} (-60) dx = -60 X_{max}$$

$X_{max} = \checkmark$

$$\omega X_{max} / N_{F_{max}} = \Delta_{FB} / \delta_{FB}$$

$N_{max}$  is a bit larger than  $N_C$  +  $N_D$

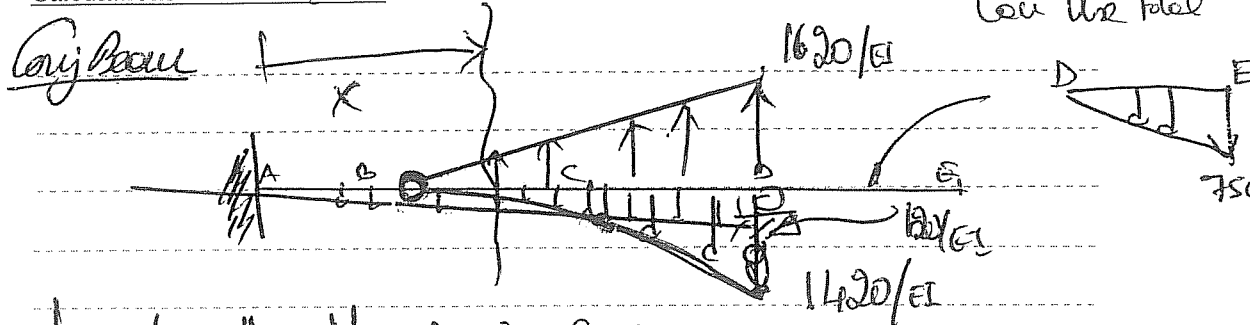
$\checkmark = 0.0048 \text{ m}$

3. USING THE CONJUGATE BEAM METHOD

Show the conjugate beam, and explain how you would compute slopes and deflection of the beam in Figure I. (10 points)



Calculations and/or Diagrams:



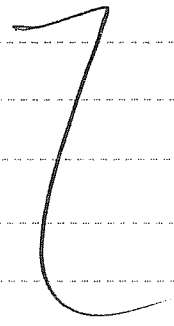
Can use total

- Load with  $\frac{M}{EI}$  of Real Beam
- Use Mom. by Parts for calculation purposes

any point x

$$\oplus \ominus \theta_{real} = V_{conj} \uparrow \oplus$$

$$\oplus \uparrow M_{real} = M_{conj} (\square \curvearrowright) \oplus$$





4. Let  $w=20 \text{ kN/m}$  and  $P=0$ .

For the same beam as in Figure 1 (with  $w$  only), and assuming member AD (Case 1) or member DE (Case 2) to be very stiff, sketch the expected deflected shape of the beam for each of the cases as shown below. (NO CALCULATIONS) (10 points)

Using the simplest and quickest approaches possible, calculate:

- (i) Case 1: the deflections  $v$  at points A and D. (5 points)
- (ii) Case 2: the deflections  $v$  at points A and C. (5 points)

DEFLECTION for Case 1

$w = 20 \text{ kN/m}$

$\Rightarrow P = \frac{20 \times 12}{2} \Rightarrow$

(i)  $N_D = \frac{P \delta^3}{3EI} = \frac{120 \times 6^3}{3EI} = 0.00432 \text{ m}$

(ii)  $N_A = \frac{1}{2} N_D = 0.00216 \text{ m}$

DEFLECTION for Case 2

$\frac{wl^2}{8} = 360 \text{ kNm}$

$N_D = 0$

$\theta_C - \theta_B = \left(\frac{2}{3}\right) \times \left(\frac{360}{EI}\right)(6) \text{ (CW)}$

$\theta_B = -\frac{1440}{EI} = -0.00072 \text{ rad}$

$N_A = |\theta_B| \times 6 = 0.00432 \text{ m} \quad (\uparrow)$

$N_C = |dBC| \times 2 = \frac{5}{384} \frac{wl^4}{EI} = 0.0027 \text{ m} \quad (\downarrow)$

$\sim$  Simple beam between B & D