

---

**Conservation of Momentum for a Linearly Accelerating Control Volume**

---

In White's book, the conservation of moment in a reference frame undergoing linear acceleration  $\mathbf{a}$  with respect to an inertial reference frame, which may be conveniently chosen to be the ground<sup>1</sup>, is given by equation (3.49):

$$\sum \mathbf{F} - \int_{CV} \mathbf{a} dm = \frac{\partial}{\partial t} \int_{CV} \rho \mathbf{u}_{/NIF} dV + \int_{CS} \rho \mathbf{u}_{/NIF} (\mathbf{u}_r \cdot \hat{\mathbf{n}}) dS$$

where

$\sum \mathbf{F}$  is the sum of forces acting on the control volume,

$\mathbf{a}$  is the acceleration of the non-inertial reference frame with respect to the inertial reference frame,

$\mathbf{u}_{/NIF}$  is the flow velocity relative to the accelerating reference frame, and

$\mathbf{u}_r$  is the flow velocity relative to the control surface.

An alternative derivation is obtained as follows. The flow velocity  $\mathbf{u}$  in the inertial reference frame may be expressed as  $\mathbf{u} = \mathbf{u}_{NIF} + \mathbf{u}_{/NIF}$ , where  $\mathbf{u}_{NIF}$  is the velocity of the non-inertial frame with respect to the inertial frame and  $\mathbf{u}_{/NIF}$  is the flow velocity relative to the non-inertial frame of reference. The conservation of momentum for a control volume fixed in the non-inertial frame is

$$\sum \mathbf{F} = \frac{\partial}{\partial t} \int_{CV} \rho \mathbf{u} dV + \int_{CS} \rho \mathbf{u} (\mathbf{u}_r \cdot \hat{\mathbf{n}}) dS$$

substituting  $\mathbf{u} = \mathbf{u}_{NIF} + \mathbf{u}_{/NIF}$ , we get

$$\begin{aligned} \sum \mathbf{F} &= \frac{\partial}{\partial t} \int_{CV} \rho (\mathbf{u}_{NIF} + \mathbf{u}_{/NIF}) dV + \int_{CS} \rho (\mathbf{u}_{NIF} + \mathbf{u}_{/NIF}) (\mathbf{u}_r \cdot \hat{\mathbf{n}}) dS \\ &= \frac{\partial}{\partial t} \int_{CV} \rho \mathbf{u}_{NIF} dV + \int_{CS} \rho \mathbf{u}_{NIF} (\mathbf{u}_r \cdot \hat{\mathbf{n}}) dS + \frac{\partial}{\partial t} \int_{CV} \rho \mathbf{u}_{/NIF} dV + \int_{CS} \rho \mathbf{u}_{/NIF} (\mathbf{u}_r \cdot \hat{\mathbf{n}}) dS \\ &= \int_{CV} \frac{d\mathbf{u}_{NIF}}{dt} \rho dV + \mathbf{u}_{NIF} \left( \frac{\partial}{\partial t} \int_{CV} \rho dV + \int_{CS} \rho (\mathbf{u}_r \cdot \hat{\mathbf{n}}) dS \right) \\ &\quad + \frac{\partial}{\partial t} \int_{CV} \rho \mathbf{u}_{/NIF} dV + \int_{CS} \rho \mathbf{u}_{/NIF} (\mathbf{u}_r \cdot \hat{\mathbf{n}}) dS \end{aligned}$$

Noting that the term between brackets is equal to zero by conservation of mass, we get

$$\sum \mathbf{F} - \int_{CV} \mathbf{a} dm = \frac{\partial}{\partial t} \int_{CV} \rho \mathbf{u}_{/NIF} dV + \int_{CS} \rho \mathbf{u}_{/NIF} (\mathbf{u}_r \cdot \hat{\mathbf{n}}) dS$$

---

<sup>1</sup>For large scale problems such as in oceanography and meteorology, earth is actually a non-inertial reference frame, but for small scale problems, it is ok to assume earth as an inertial reference frame.