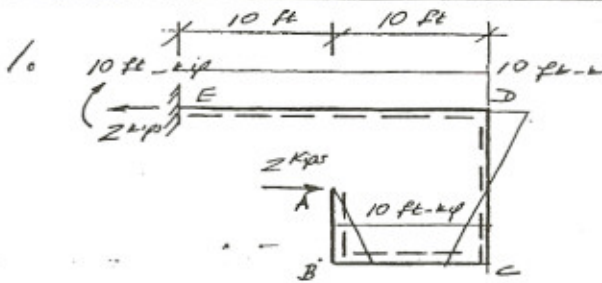
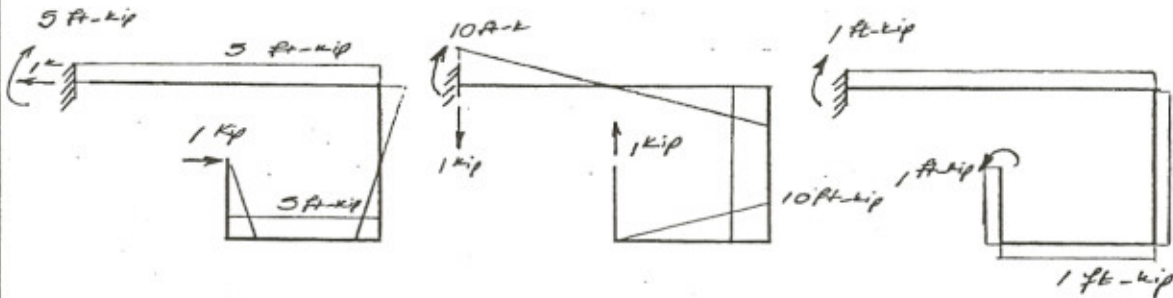


FE 1



$I = 100 \text{ in}^4$
 $E = 30,000 \text{ ksi}$



Section	Origin	Range	M_x	m_H	m_V	m_α
AB	A	0 → 5'	-2x	-1 · x	0	+1
BC	B	0 → 10'	-10	-5	-1 · x	+1
CD	C	0 → 10'	-10 + 2x	-5 + x	-10	+1
DE	D	0 → 20'	+10	+5	-10 + x	+1

$$\begin{aligned}
 U_x &= \int \frac{M_x m_H}{EI} dx \\
 &= \frac{1}{EI} \left[\int_0^5 2x^2 dx + \int_0^{10} 50 dx + \int_0^{10} (2x^2 - 20x + 50) dx + \int_0^{20} 50 dx \right] \\
 &= \frac{1750}{EI} \cdot (12)^3 \\
 &= 1.008 \text{ in} \rightarrow
 \end{aligned}$$

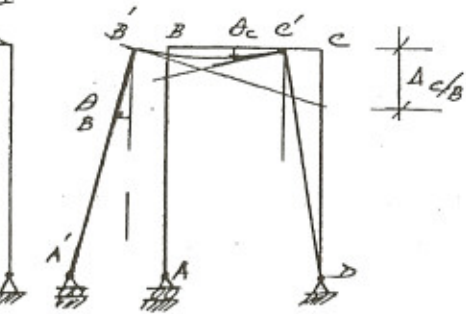
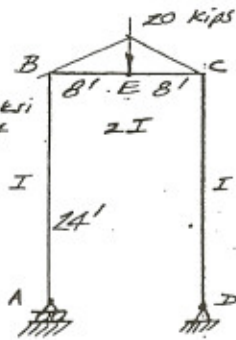
$$\begin{aligned}
 \Delta_A &= \int \frac{M_x m_V}{EI} dx = \frac{1}{EI} \left[\int_0^{10} 10x dx + \int_0^{10} (100 - 20x) dx + \int_0^{20} (10x - 100) dx \right] \\
 &= \frac{500}{EI} \cdot (12)^3 \\
 &= 0.288 \text{ in. } \downarrow
 \end{aligned}$$

$$\begin{aligned}
 \theta_A &= \int \frac{M_x m_\alpha}{EI} dx = \frac{1}{EI} \left[\int_0^5 -2x dx + \int_0^{10} -10 dx + \int_0^{10} (-10 + 2x) dx + \int_0^{20} 10 dx \right] \\
 &= \frac{75}{EI} \cdot (12)^2 \\
 &= 0.0036 \text{ rad } \curvearrowright
 \end{aligned}$$

FE I

Zo

$E = 30,000 \text{ ksi}$
 $I = 500 \text{ in}^4$



$24 \cdot \theta_B = 24 \cdot \theta_D, \theta_B = \theta_C = \theta_D$
 $24 \cdot \theta_B = 24 \cdot \theta_B$

a. Moment-Area Method

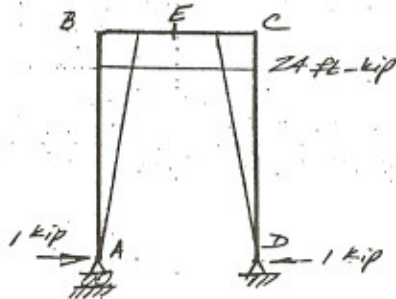
$u_A = 2(24 \cdot \theta_B) \leftarrow$

$\theta_B = \left(\frac{\Delta_{c/B}}{16 \times 12}\right) \text{ rad.}, \Delta_{c/B} = \frac{80 \text{ ft-k}}{2EI} \times \frac{16 \text{ ft}}{2} \cdot 8 \text{ ft} \cdot \left(\frac{12}{\text{ft}}\right)^3$
 $= 0.2949 \text{ in.}$

$\rightarrow \theta_B = 0.00154 \text{ rad.}$

and $u_A = 2(24 \times 12) \theta_B = 0.8847 \text{ in.} \leftarrow$

b. Virtual Work Method



Section	Origin	Range	M_x	m_H
AB	A	$0 \rightarrow 24'$	0	-x
BE	B	$0 \rightarrow 8'$	$10x$	-24
EC	C	$0 \rightarrow 8'$	$10x$	-24
CD	D	$0 \rightarrow 24'$	0	-x

$u_A = \int \frac{M_x m_H}{EI} dx = \frac{1}{2EI} \left[2 \int_0^8 (10x)(-24) dx \right]$
 $= -\frac{15360}{2EI} \cdot (12)^3$
 $= 0.8847 \text{ in.} \leftarrow$

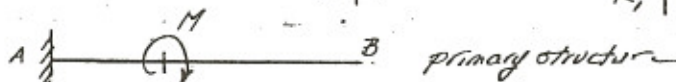
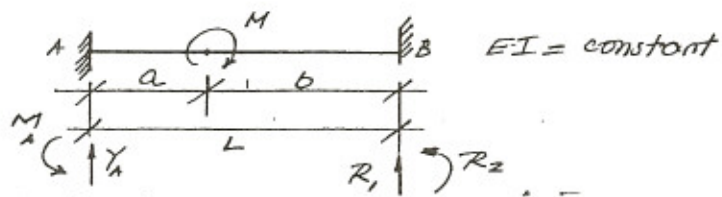
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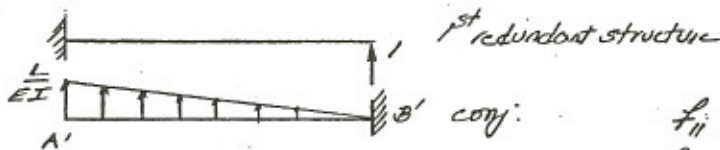
②-



$$\theta_B^I = -\frac{Ma}{EI}$$

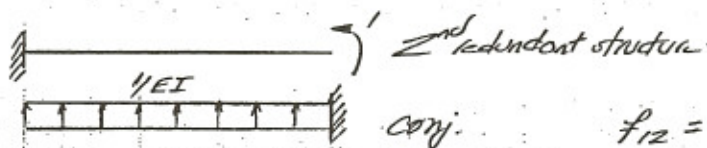
$$\nu_B^I = -\frac{M \cdot a \cdot (a+b)}{EI}$$

$$= -\frac{Ma(a+b)}{EI}$$



$$f_{11} = \frac{L}{EI} \cdot \frac{L}{2} \cdot \frac{2L}{3} = \frac{L^3}{3EI}$$

$$f_{21} = \frac{L}{EI} \cdot \frac{L}{2} = \frac{L^2}{2EI}$$



$$f_{12} = \frac{1}{EI} \cdot L \cdot \frac{L}{2} = \frac{L^2}{2EI}$$

$$f_{22} = \frac{1}{EI} \cdot L = \frac{L}{EI}$$

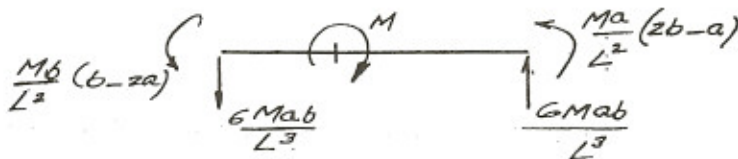
$$\nu_B^I + f_{11} R_1 + f_{12} R_2 = 0$$

$$\theta_B^I + f_{21} R_1 + f_{22} R_2 = 0$$

$$-\frac{Ma}{EI} \left(\frac{a+b}{2} \right) + \frac{L^3}{3EI} R_1 + \frac{L^2}{2EI} R_2 = 0$$

$$-\frac{Ma}{EI} + \frac{L^2}{2EI} R_1 + \frac{L}{EI} R_2 = 0$$

$$\rightarrow R_1 = \frac{6Mab}{L^3}, \quad R_2 = \frac{Ma(zb-a)}{L^2}$$

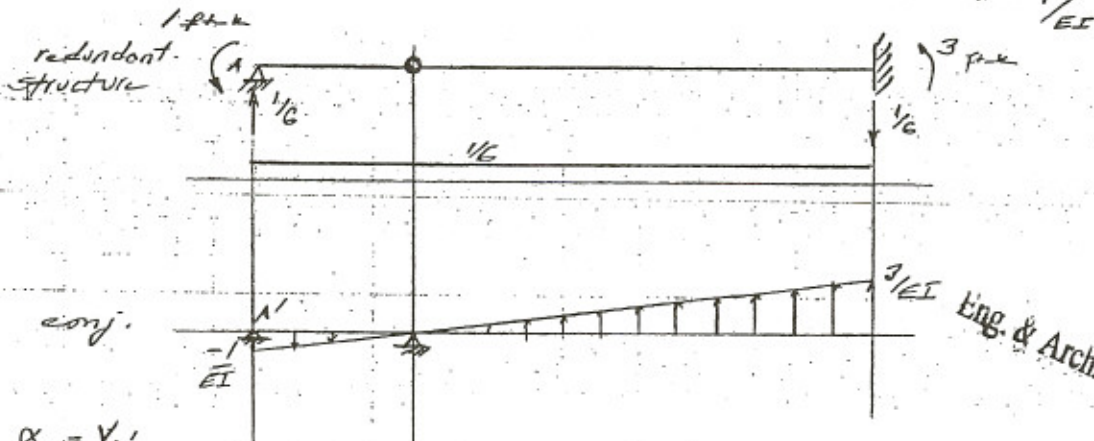
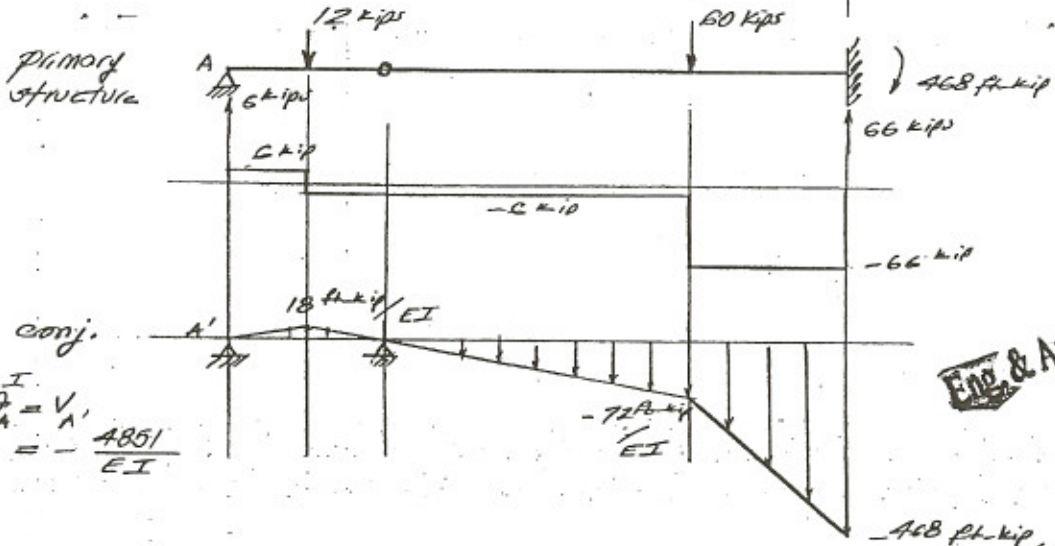
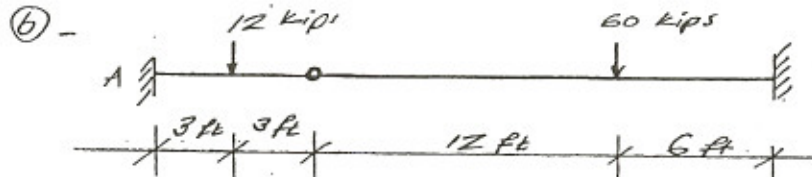


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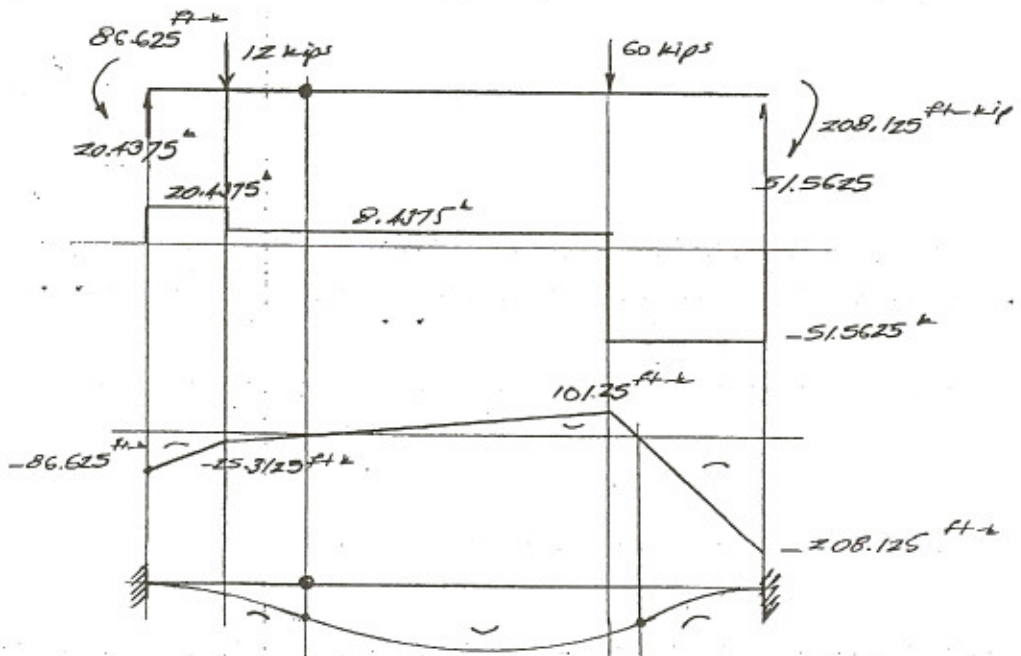
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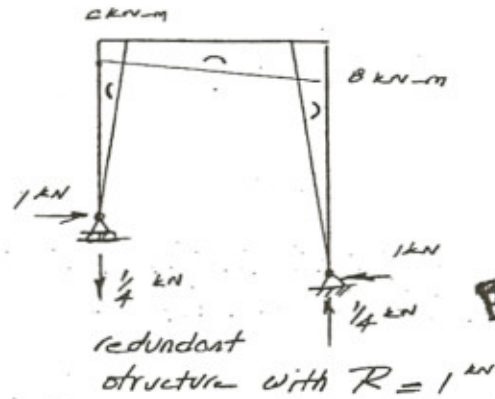
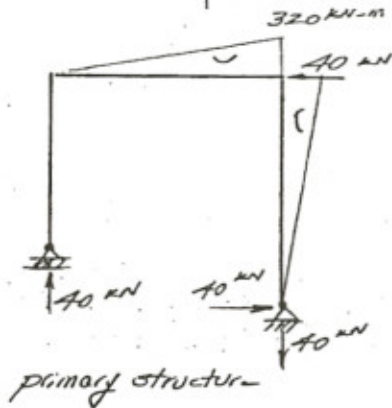
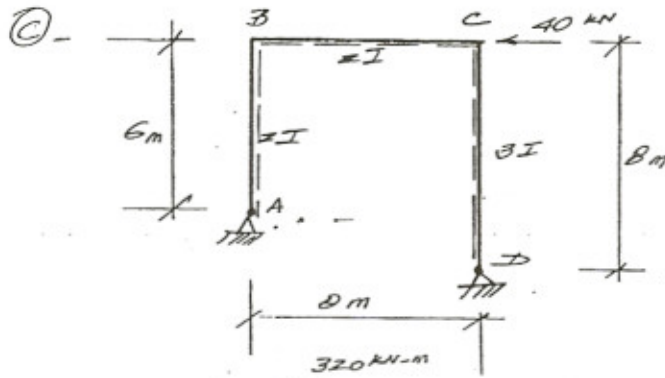
$$\theta_A^I + R \alpha_A^I = 0 \Rightarrow R = -86.625 \text{ ft-k}$$



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Section	Origin	Range	M_1	M_2
AB	A	$0 \rightarrow 6 \text{ m}$	0	$-x$
BC	B	$0 \rightarrow 8 \text{ m}$	$40x$	$-6 - \frac{x}{4}$
CD	D	$0 \rightarrow 8 \text{ m}$	$40x$	$-x$

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$$U_A^I = \int \frac{M_1 M_2}{EI} dx = \frac{1}{EI} \left[\int_0^8 \frac{(40x)(-6 - \frac{x}{4})}{2} dx + \int_0^8 \frac{(40x)(-x)}{3} dx \right]$$

$$= \frac{1}{EI} (-4693.33 - 2275.56)$$

$$= -\frac{6968.89}{EI}$$

$$U_A^{II} = R \int \frac{m_2^2}{EI} dx = \frac{R}{EI} \left[\int_0^6 \frac{x^2}{2} dx + \int_0^8 \frac{(-6 - \frac{x}{4})^2}{2} dx + \int_0^8 \frac{x^2}{3} dx \right]$$

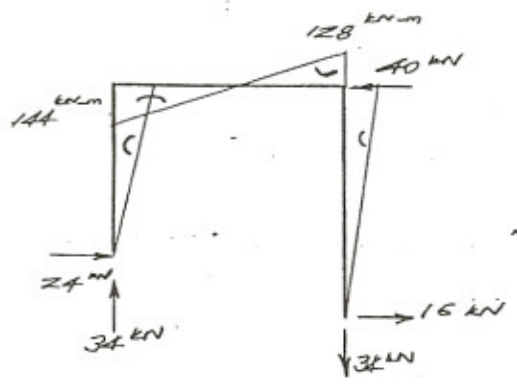
$$= \frac{R}{EI} (36 + 197.33 + 50.89)$$

$$= \frac{290.22 R}{EI}$$

$$U_A^I + U_A^{II} = 0 \rightarrow -\frac{6968.89}{EI} + R \frac{290.22}{EI} = 0 \rightarrow R = 24.01 \text{ kN}$$

$\approx 24 \text{ kN}$

FE I



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