

AMERICAN UNIVERSITY OF BEIRUT
FACULTY OF ENGINEERING AND ARCHITECTURE
ELECTRICAL AND COMPUTER ENGINEERING DEPARTMENT
EECE 442 – Communications Systems

Midterm

Closed book exam

**FOUR SHEETS OF FORMULAS WITH NO PROBLEM SOLUTIONS ARE
ALLOWED**

TIME: 1 Hour and 30 minutes

Friday, September 8, 2006

INSTRUCTOR: Dr. JEAN J. SAADE

NAME _____

ID #: _____

INSTRUCTIONS

- WRITE YOUR ID # AND NAME ON THE COMPUTER CARD, ON THIS SHEET AND ON THE SCRATCH BOOKLET IN THE PROVIDED SPACES.
- PROVIDE YOUR ANSWER ON THE COMPUTER CARD **and solution of each problem on the scratch booklet**
- **Random checking will be done to find out about any inconsistency between the problem solutions and the provided answers on the computer card.**
- RETURN THE COMPUTER CARD ATTACHED ON TOP OF THE QUESTION SHEET AND SCRATCH BOOKLET.
- **ONLY YOUR ANSWER PROVIDED ON THE COPMUTER CARD WILL BE CONSIDERED IN GRADING.**
- ALL QUESTIONS ARE EQUALLY WEIGHTED IN GRADING.

PROBLEM # 1

Consider the signal $s(t)$ in additive stationary white and Gaussian noise process $N(t)$. $N(t)$ has a mean equal to zero and spectral height $N_0/2$. The signal $s(t)$ is a deterministic finite duration energy signal defined in $[0, T]$ and having an energy equal to E . The signal plus noise are available at the input of an integrator that integrates between 0 and T . Determine the mean and variance of the Gaussian random variable, R_0 , available at the output of the integrator.

$$(a) E(R_0) = \int_0^T s(t) dt, \quad \sigma_{R_0}^2 = \frac{N_0 E}{2}$$

$$(b) E(R_0) = \int_0^T s(t) dt, \quad \sigma_{R_0}^2 = \frac{N_0 T}{2}$$

$$(c) E(R_0) = \int_0^T s(t) dt, \quad \sigma_{R_0}^2 = \frac{N_0}{2}$$

$$(d) E(R_0) = \int_0^T s(t) dt, \quad \sigma_{R_0}^2 = \frac{N_0 E}{2T}$$

$$(e) E(R_0) = \int_0^T s(t) dt, \quad \sigma_{R_0}^2 = N_0$$

PROBLEM # 2

Consider a stationary white and Gaussian noise process, $W(t)$, at the input of an ideal LPF with bandwidth equal to W rad/sec. $W(t)$ has a mean equal to zero and spectral height $N_0/2$. Let $N(t)$ be the noise process available at the output of the LPF. Select from what is given below the expression that can be the autocorrelation function of $N(t)$.

$$(a) R_N(\tau) = \frac{2N_0W}{\pi} e^{-2|\tau|} \quad (b) R_N(\tau) = \frac{N_0W}{2} e^{-2|\tau|} \quad (c) R_N(\tau) = \frac{N_0W}{2\pi} e^{-2|\tau|}$$

$$(d) R_N(\tau) = \frac{N_0W}{\pi} e^{-2|\tau|} \quad (e) R_N(\tau) = \frac{N_0W}{2\pi} e^{-2\tau}$$

PROBLEM # 3

Consider again the given in Problem # 2 and determine the mean and variance of the Gaussian random variable obtained by sampling the random process $N(t)$ at any time instant.

$$(a) E[N(t)] = 0, \sigma_N^2 = \frac{2N_0W}{\pi} \quad (b) E[N(t)] = 0, \sigma_N^2 = \frac{N_0W}{2}$$

$$(c) E[N(t)] = 0, \sigma_N^2 = \frac{N_0W}{\pi} \quad (d) E[N(t)] = 0, \sigma_N^2 = \frac{N_0W}{2\pi}$$

$$(e) E[N(t)] = 0, \sigma_N^2 = \frac{N_0W}{4\pi}$$

PROBLEM # 4

Consider the following two representations of narrow-band noise:

$$N(t) = N_c(t) \cos(\omega_c t) - N_s(t) \sin(\omega_c t) = R(t) \cos[\omega_c t + \Psi(t)].$$

Let $N(t)$ have a bandwidth equal to $2W$ rad/sec and spectral height $N_0/2$. Determine the average power of the random process available at the output of an envelope detector when $N(t)$ is available at its input.

$$(a) \frac{2N_0W}{\pi} \quad (b) \frac{N_0W}{2\pi} \quad (c) \frac{N_0W}{2} \quad (d) \frac{N_0W}{\pi} \quad (e) N_0W$$

PROBLEM # 5

Consider again Problem # 4 and determine the average power of $R(t)$.

$$(a) \frac{N_0W}{2\pi} \quad (b) \frac{N_0W}{\pi} \quad (c) \frac{2N_0W}{\pi} \quad (d) \frac{N_0W}{2} \quad (e) N_0W$$

PROBLEM # 6

Consider the following over-modulated DSB-LC signal:

$$s(t) = A_c [1 + 2 \cos(\omega_m t)] \cos(\omega_c t).$$

with $\omega_c \gg \omega_m$. Let $s(t)$ be present at the input of an envelope detector. Determine the output of the envelope detector for one period of the message signal, which is the same as the period of $\cos(\omega_m t)$. Let $\omega_m = 2\pi \times 10^3$ rad/sec.

HINT: The envelope detector output is given by:

$$\begin{cases} A_c [1 + 2 \cos(\omega_m t)], & \text{when } [1 + 2 \cos(\omega_m t)] > 0, \\ -A_c [1 + 2 \cos(\omega_m t)], & \text{when } [1 + 2 \cos(\omega_m t)] < 0. \end{cases}$$

- (a) $\begin{cases} -A_c [1 + 2 \cos(\omega_m t)], & 0.22 \text{ms} \leq t \leq 0.77 \text{ms} \\ A_c [1 + 2 \cos(\omega_m t)], & \text{otherwise.} \end{cases}$
- (b) $\begin{cases} -A_c [1 + 2 \cos(\omega_m t)], & 0.25 \text{ms} \leq t \leq 0.75 \text{ms} \\ A_c [1 + 2 \cos(\omega_m t)], & \text{otherwise.} \end{cases}$
- (c) $\begin{cases} -A_c [1 + 2 \cos(\omega_m t)], & 0.44 \text{ms} \leq t \leq 0.56 \text{ms} \\ A_c [1 + 2 \cos(\omega_m t)], & \text{otherwise.} \end{cases}$
- (d) $\begin{cases} -A_c [1 + 2 \cos(\omega_m t)], & 0.33 \text{ms} \leq t \leq 0.66 \text{ms} \\ A_c [1 + 2 \cos(\omega_m t)], & \text{otherwise.} \end{cases}$
- (e) $\begin{cases} -A_c [1 + 2 \cos(\omega_m t)], & 0.15 \text{ms} \leq t \leq 0.85 \text{ms} \\ A_c [1 + 2 \cos(\omega_m t)], & \text{otherwise.} \end{cases}$

PROBLEM # 7

Consider the generation of a DSB-SC signal by the instantaneous sampling of the message signal, $m(t)$, and the use of a BPF. It is desired to have the carrier frequency of the DSB-SC signal equal to 500KHz. Determine the sampling period, T_s , of the message signal and the maximum bandwidth, W , of the message that allows the sampling and band-pass filtering to be applied for the generation of the DSB-SC signal.

- (a) $T_s = 4 \mu\text{sec}$. $W = 500 \text{KHz}$
- (b) $T_s = 2 \mu\text{sec}$. $W = 500 \text{KHz}$
- (c) $T_s = 5 \mu\text{sec}$. $W = 500 \text{KHz}$
- (d) $T_s = 4 \mu\text{sec}$. $W = 250 \text{KHz}$
- (e) $T_s = 2 \mu\text{sec}$. $W = 250 \text{KHz}$

PROBLEM # 8

In a super-heterodyne receiver, the mixing operation is represented by multiplying the selected and amplified modulated signal, assumed DSB-SC and given by $A_c m(t) \cos(\omega_c t)$, by $\cos(\omega_p t)$. The objective is to translate the carrier frequency to a fixed IF frequency, ω_{IF} . Consider two modulated signals with frequencies $f_{c1}=1200\text{KHz}$ and $f_{c2}=900\text{KHz}$. Determine f_{p1} and f_{p2} that need to be used in the mixing operation to translate the carrier frequencies of the noted modulated signals to $f_{IF}=500\text{KHz}$.

- (a) $f_{p1}=700\text{KHz}$, $f_{p2}=400\text{KHz}$
- (b) $f_{p1}=1700\text{KHz}$, $f_{p2}=1200\text{KHz}$
- (c) $f_{p1}=500\text{KHz}$, $f_{p2}=1400\text{KHz}$
- (d) $f_{p1}=1700\text{KHz}$, $f_{p2}=1400\text{KHz}$
- (e) $f_{p1}=1700\text{KHz}$, $f_{p2}=400\text{KHz}$

PROBLEM # 9

Consider the approximated form of a NBFM signal:

$$s_{app}(t) = A_c \cos(\omega_c t) - \beta A_c \sin(\omega_m t) \sin(\omega_c t).$$

Let $\beta=0.1$ and determine the maximum deviation of the envelope of $s_{app}(t)$ from the envelope, A_c , of the NBFM signal.

- (a) $0.1A_c$
- (b) $0.005A_c$
- (c) $0.001A_c$
- (d) $0.004A_c$
- (e) $0.04A_c$

PROBLEM # 10

The bandwidth allowed for the transmission of an FM radio signal is 200KHz. Assume that the FM radio station wants to transmit a stereo message signal of bandwidth equal to 52 KHz. Determine the maximum value of the message signal. Use $k_f = 4000 (\text{V.s})^{-1}$ and Carson's rule for bandwidth computation.

- (a) 15 Volts
- (b) 10 Volts
- (c) 12 Volts
- (d) 18 Volts
- (e) 20 Volts