

Problem #1 $S = \{s_1, s_2, s_3, s_4, s_5, s_6\}$

$$P_r\{s_i\} = P_i, i=1, 2, 3, 4, 5, 6.$$

(a) $A = \{s_1, s_2, s_3\}$

$$B = \{s_4\}$$

$$C = \{s_5, s_6\}.$$

(b) $P_r(A) = P_r(\{s_1\} \cup \{s_2\} \cup \{s_3\})$

$$= P_r\{s_1\} + P_r\{s_2\} + P_r\{s_3\} \text{ since } \{s_1\}, \{s_2\}, \{s_3\} \text{ are mutually exclusive events.}$$

$$= P_1 + P_2 + P_3$$

$$P_r(B) = P_r\{s_4\} = P_4$$

$$P_r(C) = P_r(\{s_5\} \cup \{s_6\}) = P_r\{s_5\} + P_r\{s_6\}$$

$$= P_5 + P_6$$

(c) $P_r(A) + P_r(B) + P_r(C) = P_1 + P_2 + P_3 + P_4 + P_5 + P_6 = 1$

Since $A \cup B \cup C = S$ and A, B, C are mutually exclusive events. Hence,

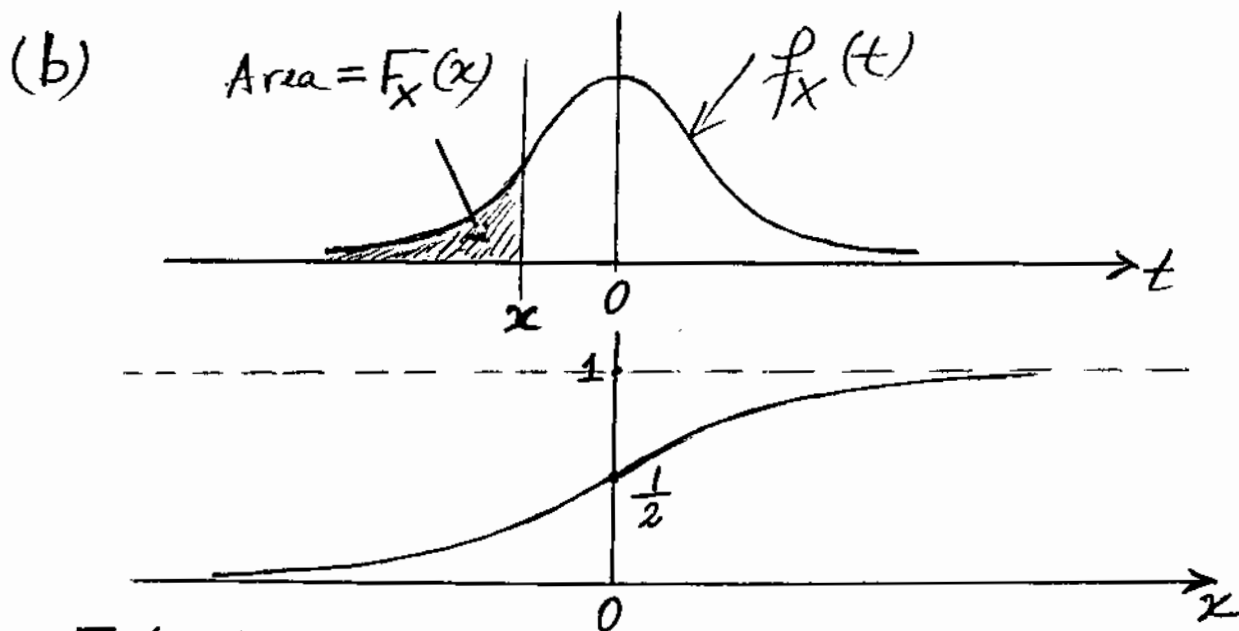
$$P_r\{(A \cup B \cup C)\} = P_r(A) + P_r(B) + P_r(C) = P(S) = 1.$$

You can also use the fact that the elementary events are mutually and their union is equal to S .

Problem # 2

$$f_X(x) = \frac{1}{\sqrt{2\pi}} \exp\left\{-\frac{1}{2}x^2\right\}, \quad -\infty < x < \infty$$

$$\begin{aligned} (a) \quad F_X(x) &= \int_{-\infty}^x f_X(t) dt \\ &= \int_{-\infty}^x \frac{1}{\sqrt{2\pi}} \exp\left\{-\frac{1}{2}t^2\right\} dt \end{aligned}$$



$$F_X(-\infty) = 0,$$

$$F_X(0) = \frac{1}{2}$$

$$F_X(\infty) = 1$$

Problem # 3

$$R_X(\tau) = E[X(t+\tau)X(t)]$$

$$= \exp\{-a|\tau|\}, \quad a > 0$$

$-\infty < \tau < \infty$

(a)

$R_X(\tau)$ as above holds for any t .

Hence, it represents the correlation between any two samples of $X(t)$ with time difference τ .

The time difference τ can be positive or negative.
 As $|\tau|$ increases; i.e., the samplers get farther away from each other, the correlation $R_X(\tau)$ decreases.
 Since $R_X(\tau) = e^{-a|\tau|}$, with $a > 0$.

(b) The process has a zero mean:

$$K_X(\tau) = R_X(\tau) - m_X^2 = R_X(\tau).$$

Hence, the samplers are uncorrelated; $K_X(\tau) = 0$, if $R_X(\tau) = 0$. \Rightarrow When $|\tau| \rightarrow \infty$ or $\tau \rightarrow \pm\infty$ the samplers become uncorrelated.

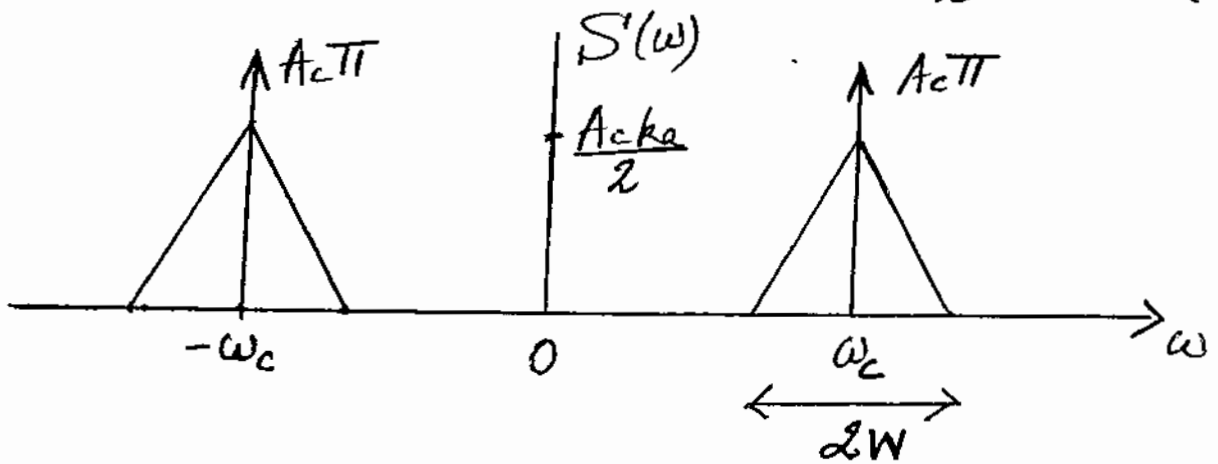
$$(c) \frac{1}{2\pi} \int_{-\infty}^{\infty} S_X(\omega) d\omega = R_X(0) \text{ average power of } X(t).$$

$$\Rightarrow \int_{-\infty}^{\infty} S_X(\omega) d\omega = 2\pi R_X(0) = 2\pi.$$

Problem # 4 $s(t) = A_c \cos(\omega_c t) + A_c k_a m(t) \sin(\omega_c t)$

$$\begin{aligned} (a) S(\omega) &= A_c \pi [\delta(\omega - \omega_c) + \delta(\omega + \omega_c)] \\ &\quad + \frac{1}{2\pi} A_c k_a M(\omega) * \frac{\pi}{j} [\delta(\omega - \omega_c) - \delta(\omega + \omega_c)] \\ &= A_c \pi [\delta(\omega - \omega_c) + \delta(\omega + \omega_c)] \\ &\quad - \frac{j}{2} A_c k_a [M(\omega - \omega_c) - M(\omega + \omega_c)] \end{aligned}$$

$$S(\omega) = A_c \pi \left[\delta(\omega - \omega_c) + \delta(\omega + \omega_c) \right] \\ + \frac{A_c k_a}{2} e^{-j\frac{\pi}{2}} M(\omega - \omega_c) + \frac{A_c k_a}{2} e^{j\frac{\pi}{2}} M(\omega + \omega_c)$$



(b) The transmission bandwidth of $S(t)$ is $2W$.

$$(c) S(t) \sin \omega_c t = A_c \cos \omega_c t \sin \omega_c t \\ + A_c k_a m(t) \sin^2 \omega_c t \\ = \frac{1}{2} A_c \sin(2\omega_c t) + \frac{1}{2} A_c k_a m(t) \\ - \frac{1}{2} A_c k_a m(t) \cos(2\omega_c t)$$

A Low pass filter of bandwidth W picks $\frac{1}{2} A_c k_a m(t)$.
Hence, a product modulator followed by a LPF can demodulate $S(t)$.

Problem # 5

The demodulation of a DSB-SC signal requires the use of a product modulator, LPF and synchronization circuitry. This is more complex than the simple use of an envelope detector followed by a LPF and a blocking capacitor.

Hence, a DSB-LC receiver is simpler and cheaper. This justifies its use commercially.

Problem # 6

$$(a) B_T = 2W(1+\beta) = 2 \times 52(1+2) = 312 \text{ KHz}$$

Hence, 312 ^{KHz} is the least separation between the transmission frequencies of adjacent FM signals based on the FDM principle.

(b) The frequency multiplication factor is:

$$n = \frac{2}{0.1} = 20.$$

Problem # 7

(a) The envelope detector input is:

$$s(t) + n(t) = A_c m(t) \sin \omega_c t + n_c(t) \cos \omega_c t - n_s(t) \sin \omega_c t$$

The envelope detector output is:

$$\begin{aligned} y_o &= \left\{ (A_c m(t) - n_s(t))^2 + n_c^2(t) \right\}^{1/2} \\ &= \left\{ A_c^2 m^2(t) - 2 A_c m(t) n_s(t) + n_c^2(t) + n_s^2(t) \right\}^{1/2} \\ &= \left\{ A_c^2 m^2(t) \left[1 - \frac{2 n_s(t)}{A_c m(t)} + \frac{n_c^2(t) + n_s^2(t)}{A_c^2 m^2(t)} \right] \right\}^{1/2} \\ &= \left\{ A_c^2 m^2(t) \left[1 - \frac{2 n_s(t)}{A_c m(t)} \right] \right\}^{1/2} \quad \text{large carrier-to-noise ratio.} \\ &= A_c |m(t)| \left[1 - \frac{n_s(t)}{A_c m(t)} \right] \\ &= \underbrace{A_c |m(t)|}_{\text{Signal Component}} \pm \underbrace{n_s(t)}_{\text{noise Component.}} \end{aligned}$$

(b) $s(t) = A_c m(t) \cos \omega_c t.$

$$\begin{aligned} \Rightarrow y_o &= \left\{ (A_c m(t) + n_c(t))^2 + n_s^2(t) \right\}^{1/2} \\ &= A_c |m(t)| \pm n_c(t). \end{aligned}$$

(c) $(SNR)_o = \frac{A_c^2 P}{\frac{N_o W}{\pi}}$