AMERICAN UNIVERSITY OF BEIRUT
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## FACULTY OF ENGINEERING AND ARCHITECTURE

## FINAL EXAM

FUNDAMENTALS OF POWER SYSTEMS ANALYSIS (EECE 471)
CLOSED BOOK (2.5 HOURS)
August 10, 2010
PROGRAMMABLE CALCULATORS ARE NOT ALLOWED.
THIS QUESTION SHEET MUST BE RETURNED WITH THE ANSWER BOOKLET.

## BRIEFLY EXPLAIN CALCULATIONS BY SHOWING FORMULAE USED.

NAME: $\qquad$ ID\#: $\qquad$

1. It is required to perform an economic load dispatch study on a system of two generators supplying a load of $P_{D}=200 \mathrm{MW}$ and connected by a transmission line, and the system losses are approximated by: $P_{L}=8 \times 10^{-4} \times\left(P_{D}-P_{\mathrm{G} 2}\right)^{2}$. The maximum and minimum active power limits of the units are given as: $40 \leq P_{G 1} \leq 160$ and $25 \leq P_{G 2} \leq 100$. The units have the following fuel-cost curves:

$$
\begin{aligned}
& C_{l}\left(P_{G 1}\right)=375+45 P_{G 1}+0.008 P_{G 1}^{2} \$ / \mathrm{h} \\
& C_{2}\left(P_{G 2}\right)=150+42 P_{G 2}+0.024 P_{G 2}^{2} \$ / \mathrm{h}
\end{aligned}
$$

a) Write the objective function and the constraints of the economic dispatch of the system with losses and use the method of Lagrange to write the necessary optimality conditions defining the saddle point (i.e. the optimum point).
b)Describe an iterative procedure based on penalty factors to solve the optimality conditions developed above and determine the active powers provided by each units $\left(P_{G 1}, P_{G 2}\right)$, the incremental cost $(\lambda)$ and the total cost of operation at the given system demand. Carry out an iteration of this procedure starting at the lossless ELD solution and determine the incremental cost at nodes 1 and 2 and the power supplied by each generator at the end of the iteration.
2. In this problem it is required to examine the solution of the load flow problem of the system of Fig. 1 using the fast-decoupled load flow (FDLF).

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Fig. 1: Transmission system for FDLF analysis.
a) Form the nodal admittance matrix of the system shown in Fig. 1.
b) Identify the type of busbars and the unknown variables that we are solving for in the system shown in Figure 1. Write the active and reactive mismatch equations to be solved in order to determine these variables.
c) Briefly describe the main characteristics of the FDLF method and how it can be derived from the Newton-Raphson method. Write the iterative FDLF equations showing the elements of the approximate Jacobian matrices for the problem being solved.
d) Carry out an iteration of the FDLF method for the equations in Part c from a set of appropriate starting values.
3. In this problem it is required to carry out a fault level analysis of the system presented in Fig. 2. The fault calculation is to be carried out at about 5 cycles following fault occurrence. System data is as follows:

Generator $\mathrm{G}_{1}: 250 \mathrm{MVA}, \mathrm{PF}=0.85,20 \mathrm{kV}, X_{d}^{\prime}=32 \%$.
Generator $\mathrm{G}_{2}: 120 \mathrm{MVA}, \mathrm{PF}=0.85,15.5 \mathrm{kV}, X^{{ }_{d}}=20 \%$.
Transformers $\mathrm{T}_{1}$ and $\mathrm{T}_{2}: 250 \mathrm{MVA}, X_{T 1}=X_{T 2}=12 \%$
Transformers $\mathrm{T}_{3}$ : $125 \mathrm{MVA}, X_{T 3}=12 \%$
Transmission line: voltage $220 \mathrm{kV}, X_{T l}=60 \Omega$ per circuit,
Load: 66 kV of 10 feeders each with a load of $30+\mathrm{j} 12$ MVA


Fig. 2: Transmission system under analysis.
a) Calculate all reactance values in per unit on 100 MVA base. Show the details of calculation of the per-unit calculations for one generator reactance, a transformer reactance, and the transmission line, and form the nodal admittance matrix for fault calculations.
b) The nodal impedance matrix, which is the inverse of the nodal admittance matrix is given below. Explain what is the significance of a diagonal element $Z_{k k}$ where $k$ is a particular node in the system? Calculate the fault current in per unit and in kA for a solid three-phase short circuit at about 5 cycles after fault occurrence at each of the nodes.

$$
\mathbf{Z}=\left[\begin{array}{llll}
j 0.1036 & j 0.0944 & j 0.0803 & j 0.0679 \\
j 0.0944 & j 0.1298 & j 0.1105 & j 0.0934 \\
j 0.0803 & j 0.1105 & j 0.1467 & j 0.1241 \\
j 0.0679 & j 0.0934 & j 0.1241 & j 0.1455
\end{array}\right]
$$

c) For a fault on one of the transmission line near node 2, calculate the fault current contributed from each generator. Which breaker(s) should "see" the fault first and clear it? Explain.
d) Using given system data, the results of Part b above, and Tables I and II of circuit breaker properties given below, select appropriate circuit breakers for the transmission line, transformers, generators, and load feeders with justification for your choice.

Table I: High Current Generator Circuit Breakers

| Type | Nominal <br> Voltage <br> $(\mathrm{kV})$ | Maximum <br> Voltage <br> $(\mathrm{kV})^{1}$ | Crest <br> Voltage <br> $(\mathrm{kV})$ | Rated <br> Current <br> $(\mathrm{kA})$ | Breaking <br> Current <br> $(\mathrm{kA})$ | Making <br> Current <br> $(\mathrm{kA})$ | Cycles |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| GB1 | $7.2-12$ | 35 | 75 | $1.2-3.5$ | $17-87$ | $40-200$ | 5 |
| GB2 | $12-24$ | 55 | 125 | $1.2-10.9$ | $12-100$ | $30-250$ | 5 |
| GB3 | $20-36$ | 75 | 170 | $1.2-4.2$ | $10-64$ | $25-160$ | 5 |

(1) Rated power frequency withstand-voltage 1 min to earth.

Table II: High Voltage Circuit Breakers (ANSI C37.06-1979)

| Type | Nominal Voltage (kV) | $\begin{gathered} \text { Maximum } \\ \text { Rated } \\ (\mathrm{kV}) \\ \hline \end{gathered}$ | Crest Voltage $(\mathrm{kV})$ | Rated Current <br> (A) | Breaking Current (kA) | Making Current (kA) | Cycles |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| HV1 | 14 | 15 | 75 | 1200 | 18 | 37 | 5 |
| HV2 | 23 | 25 | 95 | 1200 | 11 | 38 | 5 |
| HV3 | 34 | 38 | 145 | 1200 | 22 | 58 | 5 |
| HV4 | 69 | 72.5 | 325 | $\begin{aligned} & \hline 1200 \\ & 2000 \\ & \hline \end{aligned}$ | $\begin{aligned} & \hline 19 \\ & 37 \end{aligned}$ | $\begin{array}{r} \hline 37 \\ 55 \\ \hline \end{array}$ | 5 |
| EHV1 | 115 | 121 | 450 | $\begin{aligned} & \hline 1200 \\ & 2000 \\ & 3000 \end{aligned}$ | $\begin{aligned} & \hline 20 \\ & 40 \\ & 60 \end{aligned}$ | $\begin{gathered} 32 \\ 64 \\ 100 \end{gathered}$ | 3 |
| EHV2 | 230 | 245 | 850 | $\begin{aligned} & 1600 \\ & 2000 \\ & 3000 \\ & \hline \end{aligned}$ | $\begin{aligned} & 31 \\ & 40 \\ & 63 \\ & \hline \end{aligned}$ | $\begin{array}{r} 50 \\ 64 \\ 100 \\ \hline \end{array}$ | 3 |
| EHV3 | 345 | 362 | 1050 | $\begin{aligned} & 2000 \\ & 3000 \end{aligned}$ | 40 | 64 | 3 |
| EHV4 | 500 | 550 | 1425 | $\begin{aligned} & 2000 \\ & 3000 \end{aligned}$ | 40 | 64 | 2 |
| EHV5 | 700 | 765 | 1800 | $\begin{aligned} & 2000 \\ & 3000 \\ & \hline \end{aligned}$ | 40 | 64 | 2 |

