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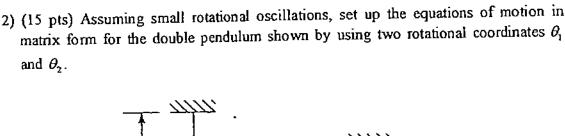
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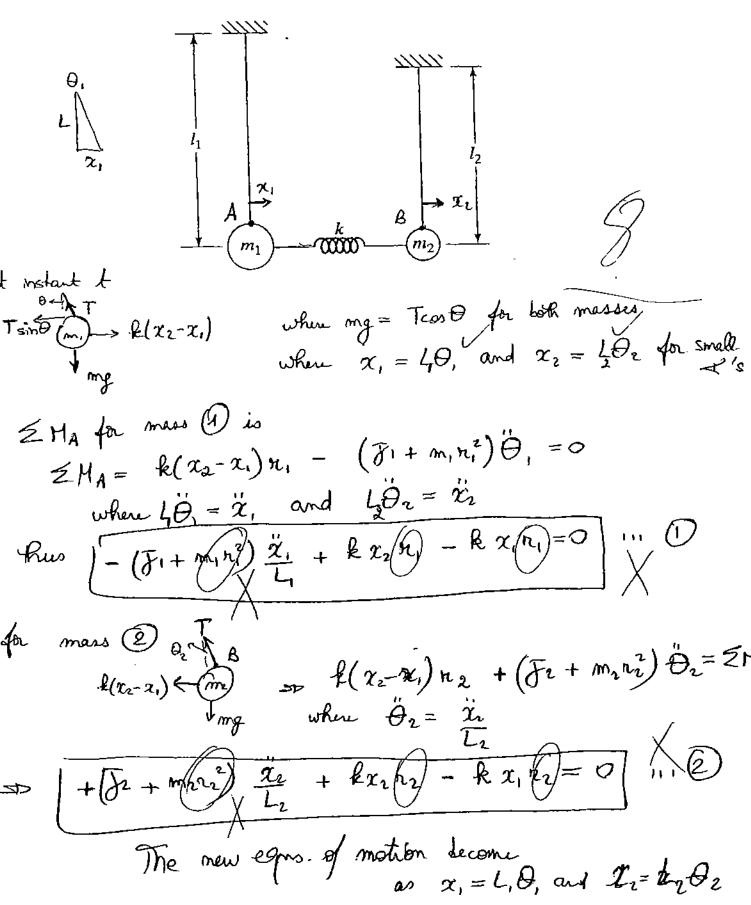
its tip can be approximated as an about the vertical axis and length and the mass of the missile and its 500kg, determine the vibration

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1) (15 pts) The wing of a fighter jet carrying a missile at its tip can be approximated as an equivalent cantilever beam with $EI = 15 \times 10^9 \, N \cdot m^2$ about the vertical axis and length L = 10m. If the equivalent mass of the wing, including the mass of the missile and its carriage system at the tip of the wing is M = 2500 kg, determine the vibration response of the wing (i.e., of M) due to the release of the missile. Assume that the force on M due to the release of the missile can be approximated as an impulse function of magnitude $\hat{F} = 50N \cdot s$.

 $3(15 \times 10^9 \text{ N·m}^2) = 45 \times 10^6 \text{ N·m}^2$ Thus the response of the why du to that impulse 2(t) = Fe-Funt sin wat wm = V King = where F = 50 N.S $cod = com \sqrt{1-5^2}$ and $J = \frac{C}{2mcom}$ in case of no damping 5=0 and cod = wn then The egn. becomes. $\mathcal{X}(t) = 1.49 \times 10^{-4} \sin 134.16t$





$$-\left(\mathcal{F}_{1}+m_{1}\eta_{1}^{2}\right)\stackrel{ii}{\Theta}_{1}+kL_{2}\eta_{1}\stackrel{\partial}{\Theta}_{2}-kL_{1}\eta_{1}\stackrel{\partial}{\Theta}_{1}=0...\left(1+kL_{1}\eta_{1}\eta_{1}^{2}\right)\stackrel{\partial}{\Theta}_{2}+kL_{2}\eta_{2}-kL_{1}\eta_{2}\stackrel{\partial}{\Theta}_{1}=0...\left(2\right)$$

$$+\left(\mathcal{F}_{2}+m_{1}\eta_{1}^{2}\right)\stackrel{\partial}{\Theta}_{2}+kL_{2}\eta_{2}-kL_{1}\eta_{1}\frac{kL_{2}\eta_{1}}{\Theta}_{2}\left(\frac{\partial}{\Theta}_{2}\right)=\left(\frac{\partial}{\Theta}_{2}\right)$$

$$-\left(\frac{kL_{1}\eta_{1}}{\Phi}_{2}+m_{1}\eta_{2}^{2}\right)\stackrel{\partial}{\Theta}_{2}+\left(\frac{kL_{1}\eta_{2}}{\Phi}_{2}+kL_{2}\eta_{2}\right)\stackrel{\partial}{\Theta}_{2}=\left(\frac{\partial}{\Theta}_{2}\right)$$

$$+\left(\frac{kL_{2}\eta_{1}\eta_{2}}{\Phi}_{2}+kL_{2}\eta_{2}\right)\stackrel{\partial}{\Theta}_{2}+kL_{1}\eta_{2}\frac{kL_{2}\eta_{1}}{\Phi}_{2}=\left(\frac{\partial}{\Theta}_{2}\right)$$

$$+\left(\frac{kL_{2}\eta_{1}\eta_{2}}{\Phi}_{2}+kL_{2}\eta_{2}\right)\stackrel{\partial}{\Theta}_{2}+kL_{1}\eta_{2}\frac{kL_{2}\eta_{1}}{\Phi}_{2}=\left(\frac{\partial}{\Theta}_{2}\right)$$

$$+\left(\frac{kL_{2}\eta_{1}\eta_{2}}{\Phi}_{2}+kL_{2}\eta_{2}\right)\stackrel{\partial}{\Theta}_{2}+kL_{1}\eta_{2}\frac{kL_{2}\eta_{1}}{\Phi}_{2}=\left(\frac{\partial}{\Theta}_{2}\right)$$

$$+\left(\frac{kL_{2}\eta_{1}\eta_{2}}{\Phi}_{2}+kL_{2}\eta_{2}\right)\stackrel{\partial}{\Theta}_{2}+kL_{1}\eta_{2}\frac{kL_{2}\eta_{1}}{\Phi}_{2}=\left(\frac{\partial}{\Theta}_{2}\right)$$

$$+\left(\frac{kL_{2}\eta_{1}\eta_{2}}{\Phi}_{2}+kL_{2}\eta_{2}\right)\stackrel{\partial}{\Theta}_{2}+kL_{1}\eta_{2}\frac{kL_{2}\eta_{2}}{\Phi}_{2}=\left(\frac{\partial}{\Theta}_{2}\right)$$

$$+\left(\frac{kL_{2}\eta_{1}\eta_{2}}{\Phi}_{2}+kL_{2}\eta_{2}\right)\stackrel{\partial}{\Theta}_{2}+kL_{2}\eta_{2}\frac{kL_{2}\eta_{2}}{\Phi}_{2}=\left(\frac{\partial}{\Theta}_{2}\right)$$

$$+\left(\frac{kL_{2}\eta_{1}\eta_{2}}{\Phi}_{2}+kL_{2}\eta_{2}\right)\stackrel{\partial}{\Theta}_{2}+kL_{2}\eta_{2}\frac{kL_{2}\eta_{2}}{\Phi}_{2}=\left(\frac{\partial}{\Theta}_{2}\right)$$

$$+\left(\frac{kL_{2}\eta_{1}\eta_{2}}{\Phi}_{2}+kL_{2}\eta_{2}\right)\stackrel{\partial}{\Theta}_{2}+kL_{2}\eta_{2}+kL_{2$$

Assuming that the tension in the massless string is constant and is equal to T, proper free-body diagram for the two masses undergoing small horizontal one by using translational coordinates x_1 and x_2 , and set up the equations of n matrix form.

for mars ()

$$1 \longrightarrow x_1$$
 $1 \longrightarrow x_1$
 $1 \longrightarrow x_1$
 $2 \longrightarrow x_2$
 $2 \longrightarrow x_2$

 $=\begin{pmatrix} 0 \\ 0 \end{pmatrix}$