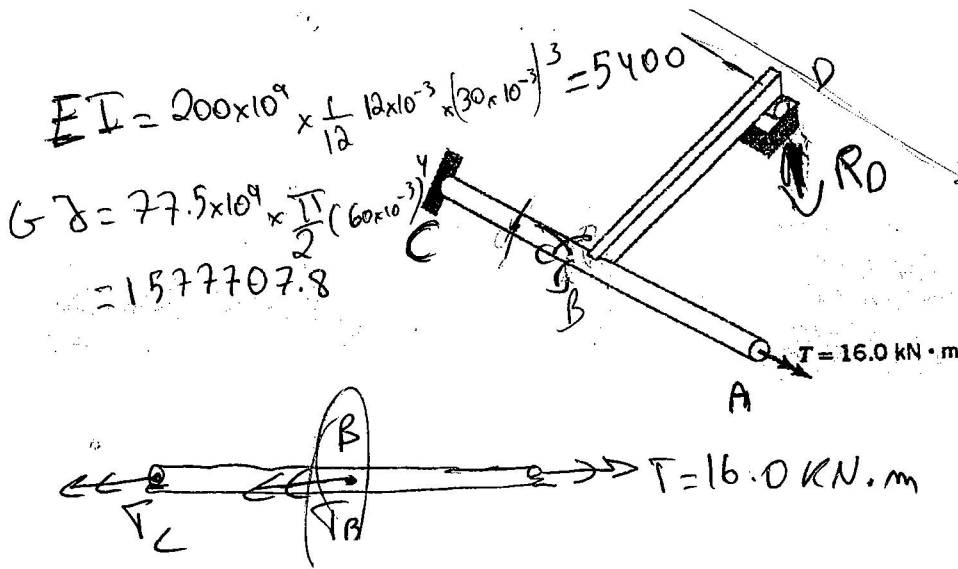


Name:

MEN 302
EXAM 2
SPRING 2006

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- 1) (20 pts) A steel torsion member has a length of 3.0m and diameter of 120mm ($E = 200\text{GPa}$, $G = 77.5\text{GPa}$). It is fixed at one end. A steel beam of rectangular cross section 120mm by 30.0mm, is welded perpendicularly to the torsion member at its midsection; as shown. The beam is supported by a roller located 2.0m from the welded section. The free end of the member is subjected to a torque $T = 16\text{kN}\cdot\text{m}$. Determine the reaction at the roller by Castigliano's theorem.



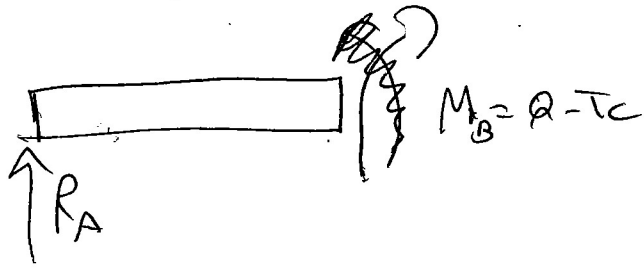
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$0 \leq x < 1.5$ $T_1 = Q$ $\frac{\delta \Phi_1}{\delta Q} = 1$

$T_C = Q - T_B$
 $T_B = Q - T_C$

$1.5 \leq x < 3$ $T_2 = T_C$ $\frac{\delta \Phi_2}{\delta Q} = 1$

On the beam;



~~$\sum M_B = 2Q - T_C$~~

$M_B + 2R_A = 0$

$Q - T_C + 2R_A = 0$

$R_A = \frac{T_C - Q}{2}$

$0 \leq x < 2m$

$M = R_A x$

$\frac{\delta M}{\delta Q} = \frac{-x}{2}$

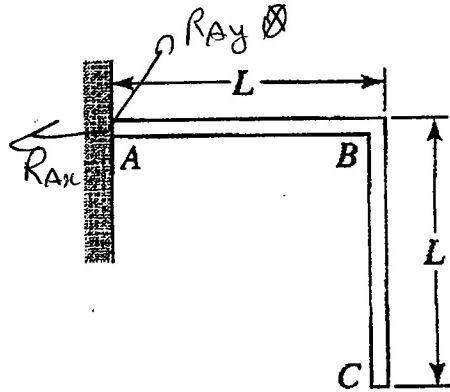
$M = \frac{T_C - Q}{2} x$

$\delta R_A = 0 = \frac{1}{EI} \int_0^{1.5} Q \cdot (1) \cdot dx + \frac{1}{EI} \int_{1.5}^3 (Q - T_B) \cdot (1) \cdot dx + \frac{1}{EI} \int_0^3 \left(\frac{T_C - Q}{2} \right) x \cdot \left(\frac{-x}{2} \right) dx$

$0 = \frac{16 \times 1.5}{EI} + \frac{1}{EI} (16 \times 3 - T_B \times 3 - 16 \times 1.5 + T_B \times 1.5) + \frac{1}{EI} \left[\frac{-T_C x^2}{4} + \frac{T_B x^2}{4} \right]_0^3$

$0 = 1.5 \times 10^{-5} + 1.5 \times 10^{-5} + \frac{T_B \times 1.5}{EI} + \frac{64 T_C}{8} \times \frac{1}{EI} + 0.02$

2) (15 pts) Member ABC lies in the plane of the paper, has a uniform circular cross-section, and is subjected to a uniform load w (N/mm) that acts perpendicular to the plane of ABC . Use Castigliano's theorem to determine the deflection of point C perpendicular to ABC . Assume that all material and cross-sectional properties are given.



~~RA~~ R_A R_C J_M

Let $R_A = Q$ $R_C = Q$

$$w \times L = F$$

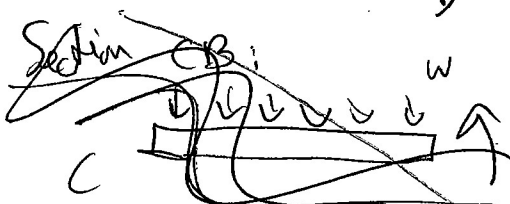


Section ~~BC~~

~~RAy~~ ~~RC~~ If we Section BC:

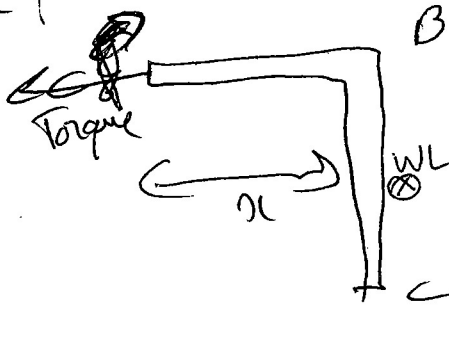
$$M_1 = R_A x + \frac{w x^2}{2}$$

$$\frac{\partial M_1}{\partial R_A} = x$$



$$M_2 = \frac{w x^2}{2} + R_C x$$

Section ABC



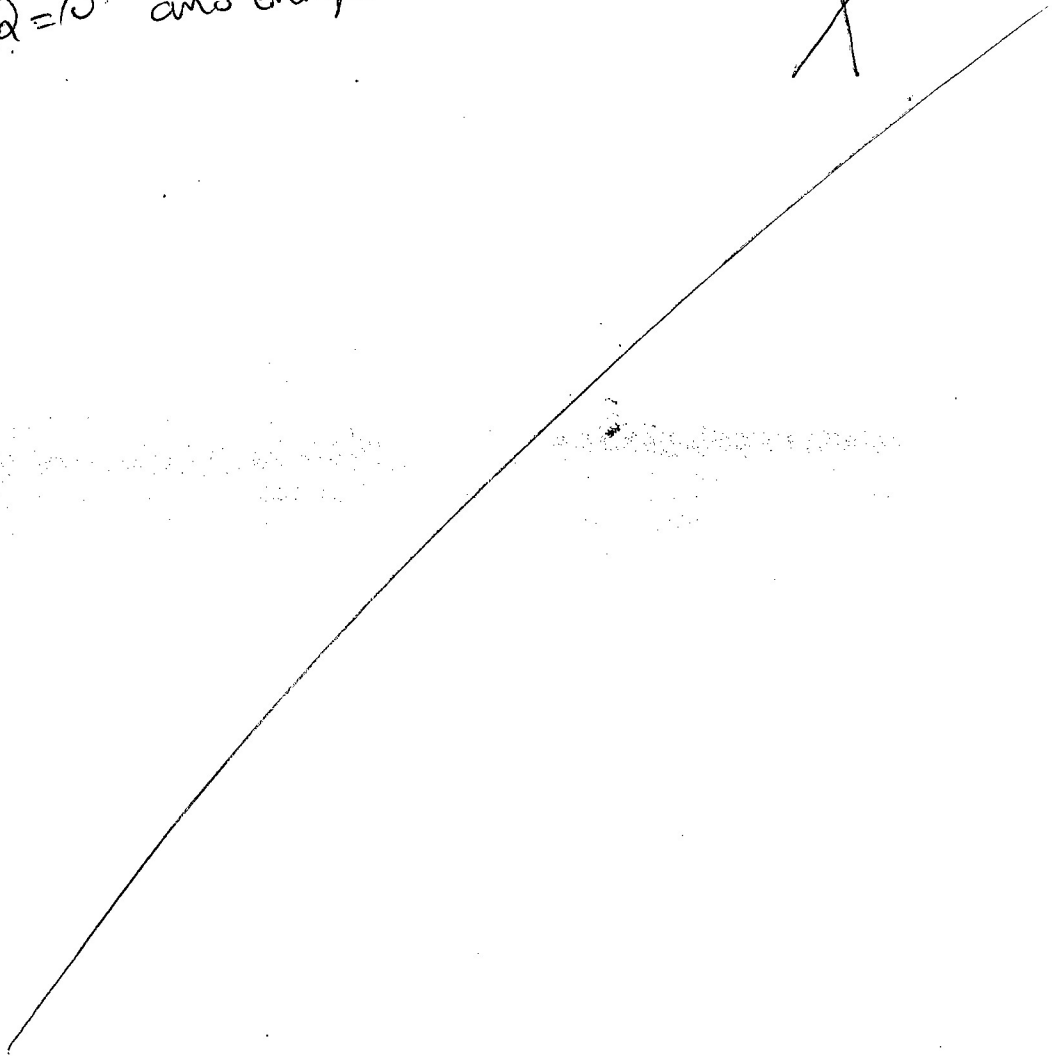
$$T = WLx + R_C x + \frac{w x^2}{2}$$

$$\frac{\partial T}{\partial R_C} = x$$

$$\delta_c = \frac{1}{EI} \int_0^L \left[Qx + \frac{Wx^2}{2} \right] [a] dx + \frac{1}{EI} \int_0^L \left[WLx + Qx + \frac{Wx^2}{2} \right] x dx$$

Set $Q=0$ and integrate

X



- 3) (15 pts) A cylinder of inner radius a and outer radius na , where n is an integer, has been designed to resist a specific internal pressure, but re boring becomes necessary. Calculate the new radius r required so that the maximum tangential stress does not exceed the previous value by more than $\Delta\sigma_\theta$, while the internal pressure is the same as before. Give your answer in terms of $\sigma_{\theta 1}$, $\Delta\sigma_\theta$, n and a .

$$a = a \quad \boxed{b = na}$$

$$\Delta r = \frac{a^2 p_i r}{E(b^2 - a^2)} \left[(1 - \nu) + (1 + \nu) \frac{b^2}{r^2} \right]$$

$$\sigma_{\theta 1 \max} = \frac{a^2 p_i}{b^2 - a^2} \left(1 + \frac{b^2}{a^2} \right) \quad b = na$$

$$\sigma_{\theta 2 \max} = \frac{r^2 p_i}{b^2 - r^2} \left(1 + \frac{b^2}{r^2} \right) \quad \text{where } r \text{ is the new radius}$$

$$\sigma_{\theta 2 \max} - \sigma_{\theta 1 \max} = \Delta\sigma_\theta \quad \checkmark$$

~~$$\frac{r^2 p_i}{b^2 - r^2} \left(1 + \frac{b^2}{r^2} \right) - \frac{a^2 p_i}{b^2 - a^2} \left(1 + \frac{b^2}{a^2} \right) = \Delta\sigma_\theta$$~~

$$\sigma_{\theta 2 \max} = \Delta\sigma_\theta + \sigma_\theta \quad \checkmark$$

but $\frac{a^3 p_i}{E(b^2 - a^2)} \left[(1 - \nu) + (1 + \nu) \frac{b^2}{a^2} \right] + a \quad \boxed{\begin{matrix} r = a \\ b = na \end{matrix}}$

but here

$$r = \text{new radius} = u \quad \frac{(u - a) E (b^2 - a^2)}{a^3 \left[(1 - \nu) + (1 + \nu) \frac{b^2}{a^2} \right]} = p_i$$

$$\sigma_{\theta_2 \max} = \Delta \sigma_0 + \sigma_0$$

$$\frac{a^2}{b^2 - a^2} p_i \left(1 + \frac{b^2}{k^2} \right) = \Delta \sigma_0 + \sigma_0$$

replace $p_i = \frac{(U - a) E (b^2 - a^2)}{a^3 [(1 - \nu) + (\nu) b^2]}$

