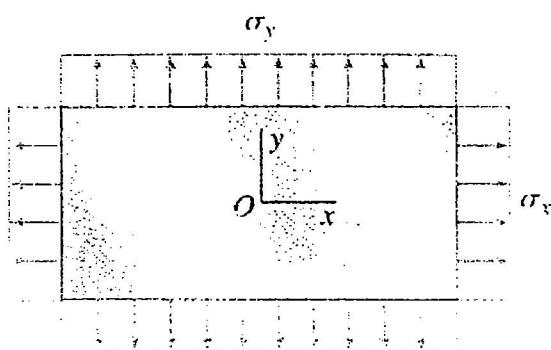


Name:

MEN 302
EXAM 1
SPRING 2004

96 good

- 1) (10 pts) A magnesium plate in biaxial stress is subjected to tensile stresses $\sigma_x = 30 \text{ MPa}$ and $\sigma_y = 15 \text{ MPa}$. The corresponding strains in the plate are $\varepsilon_x = 550 \times 10^{-6}$ and $\varepsilon_y = 100 \times 10^{-6}$. Determine Poisson's ratio ν and the modulus of elasticity of the material E .



$$\left\{ \begin{array}{l} \varepsilon_x = \frac{\sigma_x}{E} - \nu \frac{\sigma_y}{E} \\ \varepsilon_y = \frac{\sigma_y}{E} - \nu \frac{\sigma_x}{E} \end{array} \right. \quad \left\{ \begin{array}{l} E = \frac{\sigma_x}{\varepsilon_x} - \nu \frac{\sigma_y}{\varepsilon_x} \\ E = \frac{\sigma_y}{\varepsilon_y} - \nu \frac{\sigma_x}{\varepsilon_y} \end{array} \right.$$

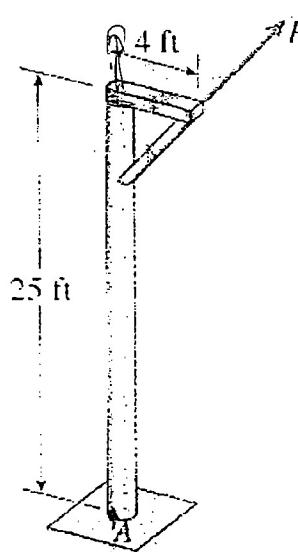
$$\left\{ \begin{array}{l} E = 5,45 \times 10^{10} - \nu (2,7 \times 10^{10}) \\ E = 1,5 \times 10^{10} - \nu (3 \times 10^{10}) \end{array} \right. \quad |0$$

$$\left\{ \begin{array}{l} E + \nu (2,7 \times 10^{10}) = 5,45 \times 10^{10} \\ E + \nu (3 \times 10^{10}) = 1,5 \times 10^{10} \end{array} \right.$$

$$\boxed{E = 4,5 \times 10^{10} \text{ MPa}} \quad \checkmark$$

$$\boxed{\nu = 0,348} \quad \checkmark$$

2) (20 pts) A post having a hollow circular cross section supports a horizontal load P acting at the end of an arm that is 4 ft long. The height of the post is 25 ft, and its section modulus (ratio of moment of inertia to distance from neutral axis to extreme fiber) is $S = \frac{I}{c} = 10 \text{ in}^3$. If the yield stress in tension and the yield stress in shear are, respectively, $S_y = 16000 \text{ psi}$ and $S_{sy} = 6000 \text{ psi}$, calculate, using both the Tresca and the Von Mises criteria, the largest permissible value of the load P by investigating the state of stress at point A, which is located at one of the poles of the cross section, as shown.



18

At point A we have :

σ_x due to bending:

$$\sigma_x = \frac{Mc}{I} = \frac{M}{S} = \frac{P \times 25 \text{ ft}}{10 \text{ in}^3} = 2.5 P \text{ ft/in}^3 \text{ psi} = 6+$$

ft/in³

τ_{xy} due to Tension

$$\tau_{xy} = \frac{Tr}{J} = \frac{4P \times c}{2I} = \frac{2P}{S} = 0.2P \text{ psi} = \tau_{xy}$$

$$\sigma_{1,2} = \frac{\sigma_x + \sigma_y}{2} \pm \sqrt{\left(\frac{\sigma_x - \sigma_y}{2}\right)^2 + \tau_{xy}^2}$$

$$= \frac{2.5P - 0}{2} \pm \sqrt{\left(\frac{2.5P - 0}{2}\right)^2 + (0.2P)^2}$$

$$= 1.25P \pm \sqrt{1.5625P^2 + 0.004P^2}$$

$$= 1.25P \pm 1.266P$$

$$\Rightarrow \begin{cases} \sigma_1 = 2,516 \text{ P (PSI)} \\ \sigma_2 = -0,016 \text{ P (PSI)} \end{cases}$$

Using Tresca criterion:

$$\tau_{max} = \frac{\sigma_1 - \sigma_2}{2} = \frac{S_{eq}}{2m} \quad (m = F_S = 1)$$

$$\frac{2,516 \text{ P} + 0,016 \text{ P}}{2} = \frac{6000}{2}$$

$$2,518 \text{ P} = 6000$$

$$\boxed{P = 2363,66 \cancel{16}}$$



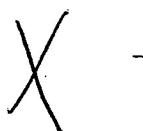
Using Von Mises criterion:

$$(\sigma_1 - \sigma_2)^2 + (\sigma_2 - \sigma_3)^2 + (\sigma_3 - \sigma_1)^2 = 2 \sigma_{eq}^2$$

$$(2,516 \text{ P})^2 + (-0,016 \text{ P})^2 + (-2,516 \text{ P})^2 = 2 (16000)^2$$

$$12,74 \text{ P}^2 = 2 (16000)^2$$

$$\boxed{P^2 = 6333 \text{ 16}}$$



So the largest value for P is: $\boxed{P = 2363,66 \text{ 16}}$



3) (20 pts) A thin-walled cylindrical tank has a mean radius of 450 mm and a wall thickness of 8.0 mm. The material has an ultimate strength of 680 MPa in tension and an endurance limit of 240 MPa. The internal pressure cycles between 1.7 MPa and 3.4 MPa. Determine the factor of safety against fatigue failure using the Von Mises criterion together with the Soderberg equation.

$$\left\{ \begin{array}{l} \sigma_{x_{min}} = \frac{P_r}{2t} = \frac{1.7 \times 10^6 \times 0.45}{2 \times 0.008} = 47,8 \text{ MPa} \\ \sigma_{x_{fat}} = 2 \times 47,8 = 95,6 \text{ MPa} \end{array} \right.$$

20

$$\left\{ \begin{array}{l} \sigma_{y_{min}} = \frac{P_r}{t} = \frac{1.7 \times 10^6 \times 0.45}{0.008} = 95,6 \text{ MPa} \\ \sigma_{y_{fat}} = 2 \times 95,6 = 191,2 \text{ MPa} \end{array} \right.$$

using soderberg criterion:

$$\left\{ \begin{array}{l} \sigma_{x_a} = \frac{1}{2} (\sigma_{x_{fat}} - \sigma_{x_{min}}) = 23,9 \text{ MPa} \\ \sigma_{x_m} = \frac{1}{2} (\sigma_{x_{fat}} + \sigma_{x_{min}}) = 71,7 \text{ MPa} \end{array} \right.$$

$$\left\{ \begin{array}{l} \sigma_{y_a} = \frac{1}{2} (\sigma_{y_{fat}} - \sigma_{y_{min}}) = 47,8 \text{ MPa} \\ \sigma_{y_m} = \frac{1}{2} (\sigma_{y_{fat}} + \sigma_{y_{min}}) = 143,6 \text{ MPa} \end{array} \right.$$

Using von Mises criterion:

$$(\sigma_{x_m} - \sigma_{y_m})^2 + (\sigma_{y_m})^2 + (\sigma_{x_m})^2 + 0 = 2 \sigma_{em}^2$$

$$5140,89 + 20565,56 + 5140,89 = 2 \sigma_{em}^2$$

$$\boxed{\sigma_{em} = 124,19 \text{ MPa}}$$

$$(\sigma_a - \sigma_y)_a^2 + (\sigma_y)_a^2 + (\sigma_x)_a^2 = 2 \sigma_{ea}^2$$

$$\boxed{\sigma_{ea} = 41,4 \text{ MPa}}$$

using solubility diagram

$$\frac{6e_a}{6a} + \frac{6e_m}{6u} = \frac{1}{F.S.}$$

$$\frac{44.4}{240} + \frac{184.18}{680} = \frac{1}{F.S.}$$

$$0.1795 + 0.1826 = \frac{1}{F.S.}$$

$$\Rightarrow F.S. = 2.815 \quad \checkmark$$